



# **amateur radio**

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# "AMATEUR RADIO"

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## FEDERAL COMMENT



### "ON GROWING UP"

Having long attained its majority, this Institute is, in many ways,  
still adolescent. In no sense is this comment to be taken as belittling  
the effort of past and present Honorary Officers of Divisions and Execu-  
tive, but is intended to be a reflection on the status and relationship of  
the Federal body to the Institute as a whole. Let us look at the present  
situation, and consider a little theory.

It is not unusual or abnormal to find that organisations or societies  
have a Head Office, with administrative and executive staff, together  
with a reasonable income collected by subscription from its members.  
If there are Divisions or Branches, it is reasonable to assume that they  
are responsible for their own affairs, and follow generally the policies  
laid down by Head Office. The finance necessary for the conduct of Branch  
affairs may, in the case of an affluent Head Office, be provided on a per  
capita basis, or by a small levy on the members of the Branch.

This, then, is the normal course of events. But what do we find  
when we look at the Institute? We find a classical example of "six tails  
wagging the dog," or, to mix the metaphor, "the part being greater  
than the whole," six Divisions all collecting a subscription and then  
forwarding the pittance of 30 cents a head to Federal Executive so that  
they can administer the complex and varied affairs of "The" W.I.A.

Surely the time has come when we must reorganise, and do some  
drastic revision of our Constitution. The amendments that have been  
proposed over the past years are steps in the right direction, but they  
do not go far enough. On the evidence available, it is obvious that  
efforts to make major changes are fraught with extreme difficulty be-  
cause of problems in some quarters. If members of all Divisions rid  
themselves of certain inhibitions and aberrations, they must then find  
themselves free to consider the reorganisation of their Head Office—an  
Executive with a paid general manager or secretary and an editor for  
their national journal who does not have to squeeze in his social and  
family responsibilities with "A.R."

This Institute has some 4,000 members in all grades, and it is not  
on the level of the "Any Town Branch of the Society for the Care of  
Anxious Felines," nor is it at A.R.L.R. status.

The day of honorary officers in the posts of Secretary and Editor of  
the W.I.A. has ceased. If they still exist, then these officers are not  
fulfilling their obligations either to their families or the Institute.

The practical benefits of implementing these proposals need not be  
stated here at this time, and to a large extent, are self evident. They  
are limited only by the imagination and resourcefulness of the man  
employed, backed up by an efficient Executive, ensuring continuity of  
effort and implementation of all policies.

It would also provide the lie to those critics who level comments  
at the Institute to the effect that it does nothing and provides even less.  
In any event, it would have been proper to fire the bullets at the critic's  
own Division. After all, how much criticism can you give at 30 cents  
a head!

—P. D. WILLIAMS, Federal Secretary, W.I.A.

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# Interference to Television and Radio Reception by Nearby Radio-Communications Transmitters

R. A. MURPHY,\* VK5ZDX, and R. S. GURR,† VK5RG

ON frequent occasions the operation of nearby radiocommunications transmitters (e.g. Taxis, Police, Amateur, etc.) causes interference to the reception of Radio or Television programmes. In rare cases this interference may be due to deficiencies in the interfering transmitter, but as the operation of these is controlled to rigid standards by the appropriate authorities, trouble from this source is not common. In such cases, no amount of work on the receiver will cure the interference, if the transmitter is radiating spurious signals in the Broadcast or Television bands.

The following types of interference may, however, confront a Radio or Television serviceman from time to time—cure may be effected in all these cases at the receiver.

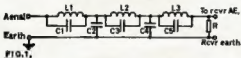


FIG. 1.

In general the mixing of the oscillator harmonics, and the unwanted signal occurs in the mixer of the broadcast receiver. The obvious cure is to stop one or other of these two signals from reaching the mixer.

The harmonic level of the oscillator in the receiver can be greatly reduced by lowering the applied voltage on the anode of the oscillator. It is wise to check the oscillator grid current as this may be excessive in some sets.

To prevent the unwanted high frequency signal reaching the mixer, better radio frequency selectivity (additional r.f. stage or the use of a low pass filter is necessary).

A typical low pass filter that will allow broadcast band signals to pass on to the receiver, but will attenuate all signals on frequencies above 1600 kcs., is shown in Fig. 1 (see "R.S.G.B.

Amateur Radio Handbook"). L1, L2, and L3 should have adjustable cores and are tuned to that L1 C1 and L3 C5 resonate at 1.8 Mcs. and L2 C3 resonate at 5.6 Mcs. Component values are: C1, C5, 330 pF.; C2, C4, 360 pF.; C3, 27 pF. L1, L3, 21.45 microhenries; 50 turns No. 32 s.w.g. enamelled wire on  $\frac{1}{2}$  in. diameter iron slugged former. L2, 71.7 microhenries; 90 turns No. 38 s.w.g. enamelled wire on  $\frac{1}{2}$  in. diameter iron slugged former. R, 400 ohms  $\frac{1}{2}$  watt. The use of an outdoor aerial in conjunction with this filter is recommended.

Direct "image" interference often occurs from signals in the 1500 to 2500 kcs. band—small ship, police, Amateur, etc., transmissions can cause trouble. If only one frequency is involved, re-alignment of the intermediate frequency amplifier to an alternative frequency will remove this problem.

Often medium frequency transmissions in the 400-500 kcs. band are picked up direct in the intermediate frequency stages—once again re-alignment of the i.f. to an alternative frequency is the cure. If it is desired to eliminate one frequency only at the aerial of the receiver, single tuned circuit may be used as a "trap". The trap (Fig. 2) is usually a parallel resonant circuit, tuned to the frequency of the interfering signal, inserted in series with the broadcast aerial, as close to the set as possible. Alternatively, a series tuned trap shunted across aerial terminal to chassis is satisfactory.

## 2.—Audio Rectification.

If the audio content of the interfering station can be heard at all points of the dial (i.e. not tuneable), it is possible that the signal is being detected in the audio frequency section of the receiver. To confirm this, the normal aerial of the receiver should be disconnected and any change in the level of the interference noted.

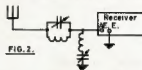


FIG. 2.

If the interference ceases, then installation of suitable traps in the aerial lead may provide a satisfactory cure. If it persists, then some work will have to be carried out on the audio circuits in the receiver.

This same effect will sometimes be noticed in radiograms even when used as amplifiers only—i.e. with the tuner turned off. This interference is caused by rectification, usually at the control grid of the first stage in the audio amplifier—i.e. the stage following the detector. Often the trouble persists irrespective of the volume control setting.

To overcome this form of rectification, it is necessary to prevent radio frequency energy from reaching the grid of this audio stage. Standard techniques for curing this are as follows—

1. Reduce grid load resistor to 2 or 3 megohms and bypass with a 250 pF. condenser. (See Fig. 3.)

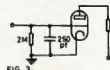


FIG. 3.

2. Insert 50,000 ohm resistor between grid resistor and grid as close to grid pin as possible—in addition bypass with 100 pF. condenser. (Fig. 4.)

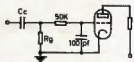


FIG. 4.

3. In some sets, audio is coupled from the detector to the first audio stage by means of cathode injection. In this case, bypassing the cathode resistor with a 100 pF. condenser will be satisfactory.

## BROADCAST INTERFERENCE

### 1.—Superheterodyne Spotting.

The harmonic radiation from the local oscillator of some broadcast sets—particularly transistor portables—is of a sufficient level to produce beats, with the nearby transmitter, that are on the same frequency as the local broadcast station. The beats are usually unnoticed on sets using an r.f. stage, where additional selectivity prevents the short wave signal from reaching the mixer stage.

A harmonic of the oscillator that falls 455 kcs. (the i.f.) away from the nearby transmitter frequency, will also cause a beat.

#### Example A:

1. Broadcast station frequency ..... 1200 kcs.
2. Receiver oscillator frequency ..... 1655 "
3. Oscillator 2nd harmonic ..... 3310 "
4. Local transmitter frequency ..... 4510 "
5. Beat between 3 and 4 1200 "

#### Example B:

1. Broadcast station frequency ..... 1200 kcs.
2. Receiver oscillator frequency ..... 1655 "
3. Oscillator 4th harmonic ..... 6620 "
4. Local transmitter frequency ..... 7075 "
5. Beat between 3 and 4 455 "

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† 19 Richmond Avenue, Colonel Light Gardens, South Australia.

In a number of cases, similar treatment to the following audio stage has been necessary to completely eliminate the trouble.

## TELEVISION INTERFERENCE

### 1.—Front End (R.F. Overload).

Because of the wide band of the t.v. station transmissions the front-end (r.f. stage) of a t.v. receiver is usually quite broad in response (minimum of 7 Mcs.). As a result, the attenuation presented to signals on frequencies on either side of the t.v. channel is not very great.

This feature is often the reason why a strong local station, operating on a nearby frequency, can cause interference to a more distant t.v. transmitter.

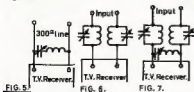
Often transmissions on frequencies quite remote from the t.v. bands may cause interference due to the same effect. In strong t.v. signal areas, the t.v. set is frequently overloaded by the t.v. transmitter often to the extent where r.f. patterning, loss of synchronization, pulling, etc., occur. This is because the a.g.c. system of the set is not correctly adjusted or in some cases not designed correctly.

In some cases, the overloaded set may produce perfect pictures, but under the influence of a nearby transmitter, r.f. patterns will be produced. As an example, an Amateur transmitter operating on 3.5 Mcs. caused interference to all channels on strong local t.v. transmissions. The transmitter was tested and it was confirmed that there were no spurious radiations in the t.v. bands. When viewing the t.v. receiver with the 3.5 Mcs. transmitter running, but the t.v. stations off the air, no interference was noted on any channel.

When a t.v. transmitter commenced operating, an interference pattern was produced on that particular channel. The cure to this trouble proved to be the insertion of a 20 db. resistive attenuator in the aerial lead-in, at the aerial terminal of the set, but often adjustment of the receiver a.g.c. control would be adequate.

A large number of cases have occurred where taxi services, Amateur stations, police transmitters, etc., have caused interference to neighbouring television reception. A number of cases have been cured by the installation of traps, tuned to the unwanted frequency, fitted to the aerial terminals of the set, but a few required installation of the traps at the feeder terminals on the t.v. turret.

The trap circuits usually consist of a small coil and a condenser in series connection (Fig. 5), but parallel tuned combinations may be used in difficult cases (Fig. 6). Sometimes a combination of both series and parallel resonant traps is necessary, as shown in Fig. 7.



Traps using 300 ohm ribbon quarter wave stub lines, and closely coupled tuned circuits made from 300 ohm ribbon in conjunction with a small trimmer condenser are also popular. Details are to be found in the various references mentioned below.

The effect of overload may vary from complete blocking of the screen through to fine wire mesh patterns. Not all r.f. patterns appearing in a t.v. screen need be caused by a nearby transmitter. Cases have occurred where the r.f. amplifier of the receiver itself has "taken off" in self oscillation and produced spurious signals throughout the r.f. spectrum. In most cases of this nature, replacement of the amplifier tube, bypass condenser, etc., in the r.f. stage will produce a cure, but often the oscillation is due to incorrect loading on the grid of the valve caused by an open circuit aerial feedline.

Audio grid rectification, as listed under "Broadcast Interference," applies equally to the t.v. set.

As a general rule, overload interference may be overcome by—

1. Overlap t.v. ribbon 2-4 inches.
2. Fit a suitable trap if the interfering signal is in the v.h.f. range.
3. Install a "high pass" filter if interfering signal is below 30 Mcs. (see Fig. 8).

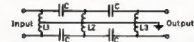


FIG. 8.  
C equals 30 uufd.  
L1 equals 40 turns centre earthed 30 gauge enamelled close wound on 1/4 inch diameter knitting needle.  
L2 equals 28 turns centre earthed 30 gauge enamelled close wound on 1/4 inch diameter knitting needle.  
(Similar high pass filters are available commercially—e.g. "Austenna".)

## AERIAL INSTALLATIONS

No radio or television receiving installation is complete without the inclusion of a "good" outside aerial. It is recognised that most modern sets are sensitive enough to give satisfactory reception with little or no aerial connected at all, but as the amount of signal induced into the set then depends more on the nature of screening and reflecting materials in the adjacent area, it is obvious any stray r.f. energy fed back into the mains (or induced into them) by nearby transmitters, will be at a level sometimes approaching that of the received signal.

The erection of a good outdoor aerial in a large number of cases has often overcome extremely aggravating cases of interference. For broadcast reception a single insulated wire running from the eaves or gable of a house to a convenient fruit tree, and oriented at right angles to the aerial of the nearby transmitter is adequate.

For television use, the "rabbits ears" or similar aerials mounted on top of the t.v. receiver rarely give satisfactory reception under normal circumstances. Flickering due to body reflections and passing vehicles, etc., are overcome when these types are replaced with a good chimney/roof mounted outdoor type. The installation of a good quality aerial inside the

roof of the house where it usually sits 8 to 12 inches above interference conducting power wiring is not satisfactory, and usually costs nearly as much as the accepted outdoor type.

Some broadcast sets are designed to work with very short aerials, and often the use of too much aerial may tax the a.v.c. system of the receiver. To overcome this and maintain the signal-to-interference improvement, overload may be corrected by cutting the aerial lead about 12 inches from the receiver and twisting the two wires together again. Alternatively, a small 2 or 10 pF. coupling condenser may be adequate.

The problem of a.v.c. in t.v. receivers can be overcome by adjusting the appropriate controls or alternatively by the installation of an attenuator. A 20 db. attenuator for installation in 300 ohm line at t.v. frequencies can be made by connecting some quarter or half watt resistors as shown in Fig. 9.

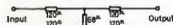


FIG. 9.

In the field, overlapping 300 ohm ribbon by 3 or 4 inches and locking the overlap with plastic adhesive tape, may be found satisfactory.

Most t.v. sets are designed to work with 300 ohm feed and consequently with resonant aerials. It is difficult therefore to expect perfect reception when a Channel 3/6 aerial combination is used to receive Channels 1/8—standing waves on the feedline can produce ghost signals and resultant "smearing," etc.

In many fringe areas, "booster" amplifiers have been installed to assist long-distance reception. Some are broadband transistorised types and are more pre-amplifiers than pre-selectors—i.e. they generally amplify everything they receive, on all frequencies. Local transmissions from nearby t.v. stations, radio-telephone transmitters, Amateurs, etc., can overload these pre-amplifiers, sometimes even though the amplifier may not be switched on, and the resultant mixture of signals fed down the feedline to the receiver.

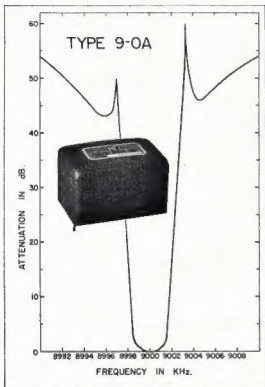
The elimination of this type of amplifier from the aerial system can do a lot to help overcome difficult interference problems. In many cases the cause of r.f. patterning on neighbouring t.v. screens has been found to be due to this type of transistorised mast-head amplifier operating in a state of self oscillation.

Servicing of an existing aerial or earth system can frequently help overcome interference problems. Loose corroded joints cause rectification and resultant mixing or re-radiation and harmonic generation. The insertion of a diode in series with an aerial is an excellent way to cause deliberate broadcast or television interference, have you considered the likelihood of crystal sets used by youngsters in the near vicinity?

Some interesting comments on the influence of aerials in broadcast reception may be found on pages 907 and 908 of the Fourth Edition of the "Radiotron Designers' Handbook."

(Continued on Page 6)





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# "THE THING"—TRANSISTORISED

## AN EXPERIMENTAL SIDEBAND EXCITER

K. A. KIMBERLEY,\* VK2PY

THESE articles are the result of a series of adventures the author experienced in the development of a transistorised sideband transceiver. How I came to be sucked into this project is not, even at this stage, really clear to me.

However, looking back over the past few months, this is how I think I was hooked. The old "idiot box" was, after all these years, fast running out of picture tube. After much procrastination, a re-gun was purchased and fitted. Much joy! We now had sound and picture again. With that chore out of the way, I thought it time something was done about my lagging interest in Ham Radio.

The first thing was to catch up on my neglected reading, yes, but how many times can you read the same jazz? Then one warm evening I casually glanced into the old junk box and my! There among the treasure trove of goodies was a box of low frequency crystals. Now what could be done with them. Ah, an idea came to mind.

Being the proud owner of a c.r.o. and a sweep generator (made to keep the one-eyed monster serviceable), I foolishly decided to play around with a crystal filter. Thinking to myself, "a few nights' fiddling around would soon convince me of the folly of it all and then I would have a good excuse to purchase a filter."

However, on this occasion "Finnagles Law†" exerted itself. The filter worked right from the beginning and this is where I really fell for the "three card trick." Could my initial success have

been a fluke? As a test, a second filter was knocked up and worked just as well.

Another experiment was now tried. The filter was re-aligned using channels 0 and 1, then channel 0 was changed to 2 and the filter re-adjusted. This took only about 60 seconds, next channel 3 was substituted for channel 1 and so on until I ran out of crystal pairs at nos. 29 and 30. In every case re-alignment from one pair to the next needed no more than about 60 seconds.

Such easy success encouraged me to go further, so then a two-section filter was constructed. Very little extra trouble was encountered here, although this was probably due to having pre-aligned the stages separately first before attempting the overall alignment.

So far OK, but of what use is a filter on its own? Logically it has to be incorporated into some equipment. Still being in the mood for experimentation, it was decided to make a transistorised sideband exciter which at some future date could be readily converted to a transceiver.

Judging by my luck previously, with the filters, this should have been a piece of cake. You know, a few transistors, a handful of small components and a 9 volt battery. Oh yeah! Three months and many cans of ale later, good, clean sideband is being produced on 3.5 Mc.

In following articles I will describe the exciter in detail as well as a brief run-down on the sweeper. If you do not own a c.r.o. and sweeper, don't despair as it is possible to use a modified g.d.o. The use of a modified g.d.o. or other bandspread oscillator is rather tedious and not to be recommended.

An explanation of the block diagram now follows. All transistors, with the exception of those used in the audio stages, are germanium PNP types with cut-off frequencies in the order of 14 Mc., i.e. OC44 types. The audio is a two-stage affair consisting of a microphone amplifier capacity coupled to a single ended output stage. The resulting audio is transformer coupled, to the balanced modulator.

The balanced modulator uses two transistors having their bases in push-pull for the audio, the emitters in parallel for r.f. and the collector push-pull for r.f.

The carrier oscillator is a common emitter crystal control oscillator and drives the emitters of the balanced modulator. The resulting oscillator output is then fed into the two-section filter. A common emitter amplifier is used in each section of the filter. Great care must be exercised here to prevent overload and hence bad signals. These amplifiers may not be needed in a straight exciter. However, as this unit is primarily intended for transceiver work, it is felt that these amplifiers would be necessary for re-aligning. The isolation provided by the transistors is helpful in alignment.

The resulting signal is now s.s.b. and now requires heterodyning to the Ham bands. Mixer circuits are notorious for the spurious signals they produce, hence it was decided to use a balanced type in an effort to reduce the spurious. As good results had already been had with my balanced modulator, it was only natural to use the same circuit configuration.

The output from the filter is single ended and, rather than make a new output transformer, a phase-splitter

(Continued on Page 8)

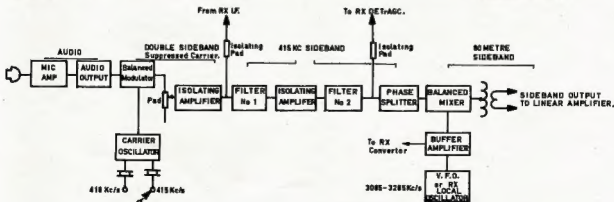


FIG. 1. BLOCK DIAGRAM.

Note: Carrier frequencies rounded out for convenience. Actuals will be quoted in following articles.  
Block diagram of an experimental sideband exciter.

### A High Stability V.f.o. for Receiver or Transmitter

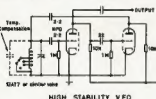
**GREG. JOHNSTON, B.Sc.**

In a recent article (January, 1966) I made brief reference to the possibility of using a V.F.O. in conjunction with the converter described, employing a fixed i.f. in the 3 Mc. range.

This V.F.O. has finally been constructed and is now in use in conjunction with a crystal filter (homebrewed) on 5327 Kc. For the benefit of any fellow s.w.l.'s, this is the set-up used in the R.D. Contest just past—the converter in a crystal locked form was the heart of the gear used in the 1965 R.D. Contest.

As the more avid readers will realise, the V.F.O. here is none other than the Franklin, not a very modern circuit but one which does not seem to enjoy a great deal of popularity at present, possibly because its output is not as high as some other types. However, for the "Like New Mexer," output is optimum with good conversion gain and low mixer noise.

The principal advantages of the Franklin oscillator are that a two-terminal coil may be used and that since voltage levels are comparatively low (a mere 70 volts h.t. on the plates) heat induced instability and drift is minimised. When this is coupled with the great inherent stability of the circuit, it could be expected that such a V.F.O. in either receiver or transmitter would be equal to the standards of performance and accuracy demanded by the more exacting type of "beats". This is in fact, the case as may be illustrated by my own experience.



HIGH STABILITY VFC

As mentioned earlier herein, using an i.f. of 5327 Kc. it was necessary to use the V.F.O. on a frequency of 9 Mc. approx. for both 20 and 80 metre reception. Taking the bull by the tail, the V.F.O. was constructed to oscillate on a fundamental frequency of this order and the results of first switching on are well worthy of mention. With a total of 35 pF. N.P.O. across the tuned circuit excluding the gang, drift from warm up was a mere few Kcs. in an hour. Compensation was very simply accomplished by placing 1.8 pF. of N750 ceramic condenser across the coil, at which stage drift was negligible after 5 to 10 minutes' warm up as shown by beating against a crystal frequency standard reference for an hour.

What about 40, 15 and 10 metre reception? Well, this is very simply accomplished by progressive shorting of pre-selected coil taps to ground so

that the circuit oscillates at 12 Mc. for 40 metres and 18 Mc. and 23 Mc. for 15 and 10 metres respectively. In other words we have a single coil grounded at one end usable on all five bands simply by tapping the inductance at the appropriate points and making provision to switch them to earth as required to permit resonance at the higher frequencies.

As with all frequency determining equipment, mechanical rigidity in construction will pay handsome dividends in performance of the finished article. In the present case this is the only "critical" component necessary as all condensers used with the exception of the 1.8 pF. N750 temperature compensating and the tuning gang, which was a ceramic type, all others were only ordinary NPO ceramic, but do not attempt to use those with a negative temperature coefficient as efficient in the coupling from the "hot" end of the coil.

## "THE THING"—TRANSISTOR'D

(Continued from Page 8)

was added between the filter and the balanced modulator. The phase-splitter worked like a charm and, at this stage, does not need further comment.

In common with most transceivers the receiver local oscillator serves as the transmitter v.f.o. On receive this oscillator mixes with the desired signal to produce an intermediate frequency which is made to be the same as our sideband generator. On transmit the reverse procedure is used, i.e. the generated low frequency sideband is mixed with the local oscillator and VOILA sideband output on the receiving frequency.

Later, I found desirable. I will add a separate v.f.o. to make it possible to transmit on frequencies other than that being received. A buffer was added between the local oscillator and the balanced mixer. This was done firstly to prevent possible frequency changes when going from receive to transmit, and secondly to boost the level going into the balanced mixer. High levels of oscillator signals here make for better sounding sideband

The generator outlined above produces 1.5v. of 80 metre sideband. This is with the output untermi-nated. Enquiries are currently being made regarding price, etc., of suitable power transistors before a decision is made on the construction of a suitable linear amplifier. The project, being of an experimental nature, was built bread-board style. Each of the main sections were made on board 6 in. x 2½ in., and when going to my satisfaction, mounted on a common base plate.

Matrix board could have been used, however, my "Scotch blood" would not allow this. Instead I used scrap 1/16 in. Laminex (bakelite sheet would be OK), drilled and eyeletted where required. Some day I hope to fit the whole into a nice-looking cabinet.

Well, chaps, that's about it for now, hope you managed to sort out the g.g. from the garbage. Next month I hope to rave on about filters and sweep generators.

## YO AWARDS

**YO-15 BY 15—WORKED 15 YO ON 15 MX**  
There are needed 15 two-way contacts with 15 YO stations on 15 mx band (21 Mc.) after 1/1/60. A YO station may be worked but once, regardless of the mode of the contact.

YO-24 Z--WORKED ZONE 20

This award is issued in three classes, for contacts made after 1/1/60 with Amateur stations of the countries belonging to Zone 30:

Bulgaria (LZ), Crete (SV), Cyprus (83B, ZC4), Dodacanese (SV), Greece (SV), Israel (4X4), Jordan (JY), Lebanon (OD5), Rumania (YO), Syria (YK), Turkey (TA) as follows:

Location Zone	Minimum number of countries worked		
	Class I.	Class II.	Class III.
15, 16, 23, 21, 34	10	8	6
14, 17, 22, 23, 33,			
35, 36, 37	8	8	4
All other Zones	6	4	2

A YO contact is obligatory in all cases.

**YO-20 BY 20—WORKED 20 YO ON 20 MX**  
There are needed 20 two-way contacts with 20 YO stations on 20 mx band (14 Mc.) after 1/1/64. A YO station may be worked but once, regardless of the mode of the contact.

### INTERFERENCE TO T.V. AND RADIO RECEPTION

(Continued from Page 3)

### EXTERNAL CROSS MODULATION

The major part of these notes has been concerned with some comments on the problems of intermodulation of signals within a receiver, and the most suitable cures. Unfortunately, from time to time cases occur where the intermodulation is external to the receiver, and location of the source is a difficult problem.

The methods and cures for this are too numerous to mention at this stage, but if an external source is suspected in any case our readers may be concerned with, check the following domestic sources:—

1. Corrosion on mains earth clamp.
2. Dry joints or loose clamps on a.c. mains entry to premises.
3. Loose fuse holders at main power board.
4. Poor or corroded junctions in conduits in electrical system.
5. Power earth wires in loose contact with gas or oil pipes.
6. Corrosion at downpipe entry into rainwater tanks, etc.
7. Gas and chip bath heater flues not completely earthed or isolated from iron roofs.
8. Presence of nearby crystal sets or t.v. masthead amplifiers.
9. Any suspected corrosion between two dissimilar metals of large dimensions.

## REFERENCE

- "Television Interference" (Second or third edition), Remington Rand, Laboratory of Advanced Research, South Norwalk, Conn., U.S.A.
- "Television Interference. Its causes and cures," by Phil Rand, 1958.
- "Radio Amateur's Handbook," A.R.R.L.
- "Amateur Radio Handbook," R.S.G.B.
- "How to Locate and Eliminate Television Interference," by Rowe (Rider Publication).
- "Radiotron Designer's Handbook," R.C.A.





for the antenna. The link winding to the emitter of the AF114N has 1½ turns of the same wire. The 270 pF. fixed condenser across the coil supplies most of the tuning capacitance required, while the variable part is provided by one section of a Roblan 415 pF. RMG2 which has a 100 pF. fixed capacitor in series with it to restrict the tuning range.

A.v.c. is applied to the r.f. stage via the 5.6k resistor in the base circuit, while back-to-back OA91 diodes are used across the input to provide some measure of front-end protection.

#### Mixer

L11, the interstage coupling transformer, is also wound on a Ducon Q2 miniature pot core. The tuned winding again consists of 13 turns of 29 B. & S. wire. The base link has 1½ turns of the same sized wire. The second section of the 415 pF. Roblan twogang is also padded with a 100 pF. capacitor to restrict the frequency range.

Oscillator injection is via the 1000 ohm and 0.01 µF. 25 volt condenser in the emitter circuit.

#### I.F. Transformer

L9 and L10 are the two top-coupled transformers. Each is wound on a Ducon Q1 miniature pot core and each consists of an 84-turn winding of 36 B. & S. wire. In L10 the collector tap is 22 turns from the cold end (i.e. -7.5v. feed end) while L9 is tapped at 12 turns from the cold end.

As in the four preceding stages the whole unit is built on to a printed circuit board specially made for the project.

At some later date—probably in the new year—the results obtained when testing the completed receivers will be published. Also around that time it is hoped to publish details of the h.f. converters now being designed. At a still later stage—and if warranted by the demand—the Moorabbin Club will be following this project with a side-band generator. Two such units are now being developed—one on 455 Kcs. using a mechanical or ceramic filter, and one on 9 Mcs. using a four-crystal filter.

This article then concludes the first phase of the Moorabbin project.

Although for convenience the writer's name has appeared on this series of articles, it must be emphasised that the running of the project has been a team affair. Bob VK3AKJ, Ken VK3AFJ, Bert VK3AAF and Col VK3XV have been assisting on the procurement side, Neil VK3ZRT and Ken VK3AKK have been the main strengths on the technical and "trouble-shooting" front, Eddie VK3EM has spent countless hours on the many drawings involved, Jim VK3KE has provided the hundreds of drawing reproductions required, Peter VK3XK has borne the full weight of setting up and duplicating the instructions, while Ron VK3RN and Lindsay VK3ZNS have spent many evenings making up the kits.

The project as a whole has been of far greater interest than was originally envisaged. When first mooted the committee estimated that, perhaps, 20 members would take part. At the moment there are no less than 73 participants from all states and a couple from ZL.

What's next?—N.F.D. of course!

★

## NATIONAL FIELD DAY RULES

The Rules of the Field Day of 11th and 12th February, 1967, will be the same as those of 1966, which were published in "A.R." of December, 1965, except for:—

(1) Crossmode operation is permitted, and will count for scoring purposes.

(2) Fixed Stations working Mobile/Portable will be eligible for Certificates.

★

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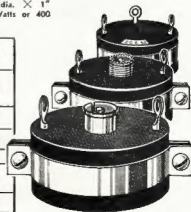
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351A	Impedance ratio 1:4. 75 ohms unbalanced to 300 ohms balanced. 3 to 30 Mc/s. For use at centre of a folded dipole antenna with coaxial feed line or at base and with 300 ohm twin line connector and terminals as 350A.
352A/BC	Details as 350A except freq. range 500 Kc/s. to 5 Mc/s. or to 30 Mc/s. for receiving purposes only with increased attenuation.
353B	This is a type 350 with a coaxial socket SO 239 (Amphenol screw type).
354B	Type 351 with SO 239 coaxial socket.
355C	Impedance ratio 2:1. 50 ohms unbalanced to 25 ohms unbalanced. 3 to 30 Mc/s. For use at the base of a mobile whip antenna, coupled to fixed or adjustable transmitter output impedance. Lug terminals.
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# TRANSISTOR AMPLIFIER DESIGN

## PART THREE

R. L. HARRISON,\* VK3ZRY

**T**HIS article will cover class A, large signal, audio amplifiers. I will first discuss classes, limitations and requirements that have to be considered before setting out a design method. The method itself is, of necessity, graphical and thus, before attempting to design an audio power amplifier, you must obtain the base and collector characteristic curves. That is  $I_c$  versus  $V_{ce}$ ,  $I_c$  versus  $V_{be}$ , and  $I_b$  versus  $V_{be}$ . Some basic knowledge of transistors and transistor terminology is assumed.

### CLASSES OF AMPLIFIERS

Amplifiers, r.f. or a.f., are divided into four classes. These classes are defined by the operating conditions under which the amplifiers operate. The four classes are designated A, AB, B and C. For audio work we will be interested in classes A, AB and B.

**Class A:** The base-emitter bias is set so that collector current flows at all times.

**Class B:** The base-emitter bias is set to approximate collector cut-off so that collector current flows for only 180° of the input cycle.

**Class AB:** The base-emitter bias is set between class A and class B. Collector current flows for more than 180° but less than 360° of the input cycle.

Class A amplifiers are used where linearity or freedom from distortion is the main requirement, but efficiency is low. Typical efficiency for transistors is from 20% to 35%. Maximum theoretical efficiency is 50%.

Class B amplifiers are extremely efficient and provide high power output. With transistors, the inherent linearity of the collector characteristics gives low distortion figures not normally encountered with tubes. Efficiency is typically 70 to 75%, which makes this configuration very attractive for mobile. Maximum theoretical efficiency is 78.5%.

Class AB amplifiers give more power output than class A but less distortion and power output than class B. With transistors, the difference in distortion figures between class B and class AB is so small as to be only a minor criterion. Typical class AB efficiencies approach 60%.

### LIMITATIONS AND REQUIREMENTS

For audio work only, class A amplifiers can be used in a single ended stage. Class B must be used in push-pull arrangements because a single stage would have severely distorted output as the transistor is conducting only over portion of the input cycle.

For all classes of operation the power output is limited by:—

- Maximum power dissipation rating ( $P_{Dmax}$ ). This depends on the ambient temperature and design of the cooling system.

- Maximum collector to emitter voltage ratings ( $V_{CEmax}$ ). This rating is generally due to the zener breakdown of the collector-base junction.

- Maximum emitter current rating, or more usually, maximum collector current rating ( $I_{Cmax}$ ). This depends on the fall-off of  $h_{FE}$  with increasing emitter current.

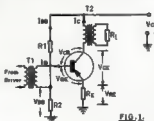
In designing an amplifier we must check that none of these ratings are exceeded at any time.

One of the main requirements of audio power amplifiers is thermal stability. In most cases (low power) this is readily obtained by normal biasing methods similar to that outlined in Part 1. The exception here though is that the bias components' bleed current is relatively high and the emitter resistor  $R_E$  is very low or non-existent. By-passing of  $R_E$  or  $R_E$  is not often encountered as little signal is lost in these components and by-pass capacitor values would be impractical.

Complementary to thermal stability is the prevention of, and compensation for, temperature rise. A good heat-sink and adequate cooling facilities should be provided, keeping in mind the power involved. Temperature compensation will be discussed fully later.

### CLASS A DESIGN

Fig. 1 gives the circuit suitable for class A, low to medium power applications. Note that it is a single ended stage—push-pull comes later.



The first thing you have to do is obtain several sets of different transistor characteristics. Now, assuming you have several suitable base and collector characteristics, you can follow the procedure set out below.

- Choose peak power output ( $P_o$ ) required to be delivered to the load and add 20% (one-fifth) to account for losses.
- Calculate  $P_{Cmax}$  from following equation:  $P_{Cmax} = Z P_o + \frac{1}{2} P_o$ .
- Choose  $V_{CE}$  (collector supply voltage). You will probably already know what this is to be. Check that  $V_{CE}$  is greater than or equal to  $\frac{1}{2} V_{CEmax}$  (where  $V_{CEmax}$  is to be taken from manufacturer's data).

This is because the instantaneous collector voltage swings to twice  $V_{CE}$  on signal peaks.

- Now choose your transistor, keeping in mind the limitations set out

above. The  $P_{Cmax}$  value found in No. 2 above should be equal to or, preferably, somewhat less than  $P_{Cmax}$  of the transistor you select. This criterion will be your deciding factor. Gain of the transistor is another consideration and I will leave that up to you.

- Using the value of  $V_{CE}$  chosen in No. 3, calculate your working point (quiescent or Q-point) collector current ( $I_{CQ}$ ) from this equation:—

$$I_{CQ} = \frac{Z P_o}{V_{CE}}$$

where  $I_{CQ}$  is in amps.

$V_{CE}$  in volts.

$P_o$  is the power output required plus 20%, in watts. From now on  $P_o$  is this value.

6. The junction of  $I_{CQ}$  and  $V_{CE}$  on the collector characteristics determines your Q-point (see Fig. 2). Now draw a straight line from  $2 \times I_{CQ}$  through the Q-point to  $2 \times V_{CE}$ . This is your a.c. (signal) load line which will give the power output you desire, unless of course you have made a mistake. Unfortunately, mistakes made here will not be discovered until later.

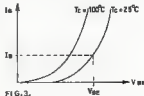


- Determine your operating base current ( $I_{BQ}$ ) at the Q-point.

The Q-point will come near or on one of the collector characteristics which will be marked with a certain base current (see Fig. 2). If the Q-point falls on a line, then you are lucky; the value marked on this line will be your operating base current. If the Q-point is between two lines, you will have to figure out approximately what your base current  $I_{BQ}$  isn't be too accurate, it is not necessary.

- Determine your base-emitter voltage  $V_{BEQ}$  from the base characteristics ( $I_b$  versus  $V_{BE}$ ), see Fig. 3.

Look up the  $I_{BQ}$  axis to the value of  $I_{BQ}$  found in No. 7, project a line across to the appropriate curves for different temperatures—assume  $T_c = 25^\circ C$ , unless you wish to run your transistor at



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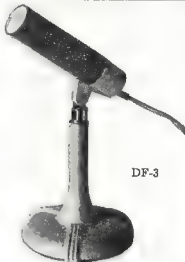
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 (C) Telephone Drainage Coil,  
 (D) Telephone Longitudinal Retard Coil



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a higher temperature. Now drop a line down to the  $V_{BE}$  axis and this is your value for  $V_{BE}$ .

Another way is to look up the graph of  $I_C$  versus  $V_{BE}$  (see Fig. 4). Find your collector current value ( $I_C$ ) on the  $I_C$  axis, project a line across to the appropriate curve ( $T_C = 25^\circ\text{C}$ .) and another line down to  $V_{BE}$  from the curve (Fig. 4).

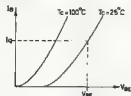


FIG. 4.

9 Now we have to consider our bias and stabilisation components.

So that only a small loss occurs in  $R_2$  and  $R_1$ , their resistances should be low. In practical circumstances we find that  $V_{BE}$  is one-tenth or less of the collector supply voltage ( $V_{CC}$ ).

This ensures that  $R_2$  has a low value and yet provides part of the bias voltage we need and also reduce changes in forward conduction due to a rise in temperature.

Calculate  $R_2$  from the following formula:—

$$R_2 = \frac{V_{CC}}{10 I_C}$$

where  $R_2$  is in ohms.

$V_{CC}$  in volts.

$I_C$  in amps.

Use a resistor of proper power rating; this being given by:—

$$P_{R2} = V_{R2} \times I_C \text{ watts.}$$

You can make  $R_2$  higher than this value for better thermal stability, but the bias and stabilisation components discussed here will only serve over a limited temperature range. More will be said about this in Part 4 on class B amplifiers.

10. To calculate  $R_1$  and  $R_2$ , use the following formulae (refer to Fig. 1):—

$$\text{Let } I_{B2} = 10 \times I_C$$

$$\text{then } R_2 = \frac{V_{CC} - V_{BE}}{I_{B2}}$$

where  $R_2$  is in K ohms  
if  $V_{CC}$  and  $V_{BE}$  in volts  
and  $I_{B2}$  in milliamperes.

$$\text{Now } R_1 = \frac{V_{CC} - V_{BE}}{I_{B2} + I_C}$$

where  $R_1$  is in K ohms  
if  $V_{CC}$  and  $V_{BE}$  are in volts,  
 $I_{B2}$  and  $I_C$  are in milliamperes.

At this point check to see that  $V_{CE}$  max. is not exceeded:—

$$V_{CE} \text{ max.} > V_{CC} - V_{BE}$$

Those are the ten steps for setting up the d.c. and part of the a.c. conditions necessary for the proper operation of your chosen transistor. The next thing is to determine the turns ratio of  $T_1$  and  $T_2$  and the power required to drive the stage adequately.

#### Output Transformer $T_2$

Let us take a look at what loads the output transformer  $T_2$  has to match (see Fig. 5).



FIG. 5.

The load on the secondary,  $R_L$ , may be a speaker or the modulating impedance of the p.a. of a transmitter. The primary load,  $R_{L1}$ , is the effective load presented to the transistor collector to produce maximum power output.  $R_{L1}$  is actually the reciprocal of the slope of the a.c. load line found in No. 6 previously.

Therefore:—

$$R_{L1} = V_{CE} / I_C$$

$$\text{or } R_{L1} = V_{CE}^2 / 2 P_o$$

The turns ratio is then given by:—

$$N_1 + N_2 = \sqrt{R_{L1} + R_L}$$

Now you can either obtain a transformer suitable for the purpose or design your own. Designing your own transformer would take an article in itself and, as this has already been done, I'll refer you to an excellent book, Bernard's Radio Manual, called "Coil Design and Construction." It is quite cheap and easy to follow—it would also come in handy for Part 2 of these articles.

#### Input Transformer $T_1$

2. The input transformer  $T_1$  is a different kettle of fish. In some cases it is not necessary to have one and a capacitor input can be provided (see Fig. 6).

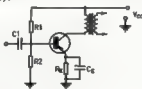


FIG. 6.

$R_1$ ,  $R_2$ ,  $C_1$ ,  $C_2$  and  $R_L$  are found from Part 1 of these articles and the transistor and transformer found as outlined above.

3. The arrangement in Fig. 6 is suitable for transistors delivering up to 300 mW. output. If more than this is desired from a single ended output stage a transformer input must be used as in Fig. 1.

We can represent the driver transistor, the transformer  $T_1$  and the input circuit of the output transistor by the equivalent circuit in Fig. 7.

$R_1$  and  $R_2$  are neglected—assumed negligible. The two rings crossing each other represent a constant current generator (e.g. a transistor).

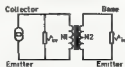


FIG. 7.

$r_{ce}$  = Collector-emitter signal resistance of driver transistor.

$r_{be}$  = Signal input resistance of output stage.

Now  $r_{be}$  can be obtained from the formula:—

$$r_{be} = \frac{V_{BE}}{I_B}$$

where  $V_{BE}$  = Base-emitter signal voltage swing (peak to peak).  
and  $I_B$  = Base current swing with signal (peak to peak).

The value of  $V_{BE}$  can be found from the collector current versus base-emitter voltage curves (see Fig. 8). Unless you plan to operate at a high temperature assume  $T_C = 25^\circ\text{C}$ . ( $77^\circ\text{F}$ .)

Now you will know your collector current swing (C to D on Fig. 2). Project the values across to the appropriate curve (Fig. 8) and down to the  $V_{BE}$  axis. By subtracting  $V_{BE}$  min. from  $V_{BE}$  max. you will find  $V_{BE}$ .

The value of  $I_B$  can now be found by subtracting the value of  $I_B$  at point C in Fig. 2 from the value of  $I_B$  at point A.

i.e.  $I_B$  at C = 10  $\mu\text{A}$ .

$I_B$  at A = 80  $\mu\text{A}$ .

then  $I_B = 70 \mu\text{A}$ . (p.p.).

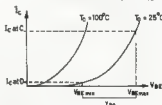


FIG. 8.

The value of  $r_{ce}$  (Fig. 7) must be known to enable us to determine the turns ratio of the transformer from the formula:—

$$N_1 + N_2 = \sqrt{r_{ce} + r_{be}}$$

The method above (1 to 10) can be used to select a driver transistor but first the power needed to drive the output stage must be known as this is the first criterion. The power input to the output stage is given by:—

$$P_i = v_{be} \times I_B \times 1.5$$

(multiply by 1.5 to account for losses, etc.)

using the values of  $v_{be}$  and  $I_B$  calculated above.

After designing your driver stage up to number 5,  $r_{ce}$  can be found from the formula:—

$$r_{ce} = \frac{V_{CC}}{I_C (\text{driver})}$$

Knowing this will then enable you to calculate the turns ratio of the driver transformer.

#### PUSH-PULL CLASS A AMPLIFIERS

For proper operation of the amplifier in Fig. 9 the circuit must be electrically symmetrical. That is, the base currents, base signal voltages, base bias voltages, emitter resistors, collector currents and voltages must be arranged so as to produce identical output signals across each half of the primary of  $T_2$ .

It sounds like a tall order but it is not very difficult to produce and the advantages are great.

The advantages of push-pull operation are:—



- (a) More than twice power output over single ended stage for a given distortion.
- (b) Even harmonics cancelled in output
- (c) When driven hard produces less distortion than a single ended stage.
- (d) Ripple voltage on  $V_{cc}$  line does not appear in output owing to cancellation in output transformer.
- (e) Output transformer less bulky for same power output from a single ended stage.

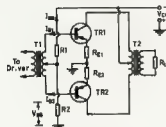


FIG. 9.

The disadvantages are:—

- (a) Some difficulty can be experienced in trying to obtain gain-matched transformers.
- (b) Requires more components and centre-tapped transformers.
- (c) Draws more current from the supply than a single ended stage.

The design of a push-pull stage follows very closely that of a single ended stage.

Modifications to the procedure are as follows (refer to Fig. 9):—

1.  $P_o$  max. of T1 or T2 =  $P_o$ . Power output ( $P_o$ ) having first been determined, this takes the place of No. 2 in method outlined above.
2. For calculating R1 and R2 use the following equations instead of those in 10 above:—

Now we assume  $I_{sa} = 10$  ( $I_{s1} + I_{s2}$ ) therefore  $I_{sa} = 20$  ( $I_{s1}$ )—assuming base currents approx. equal.

$$\text{Now } R2 = \frac{V_{sa} + V_{s21}}{I_{sa}}$$

$$\text{and } R1 = \frac{V_{cc} - V_{s21}}{I_{sa} + 2 I_{s1}}$$

(assuming symmetry).

3. The design of the output transformer will have to be modified slightly. The circuit of Fig. 7 can be modified to that in Fig. 10.



FIG. 10.

For symmetry,  $N1 = N3$ .

The turns ratio is given by:—

$$N1 \div N2 = \sqrt{R_{L21} \div R_L}$$

$R_L$  = Load on secondary (speaker or mod. impedance of tx).

$$R_{L21} = (V_{os} \div I_{s1}) \text{ for } T_{s1}$$

Now, seeing as both sides are symmetrical (we hope),

$$R_{L21} = R_{L22} = V_{os} \div I_{s1} \text{ (for } T_{s1} \text{ or } T_{s2}).$$

So the turns ratio can be easily found and the primary turns either side of the centre tap will be equal. It is suggested that the primary be bifilar wound. The start of one wire is connected to the finish of the other to provide the centre tap. The reasons for winding the primary in a bifilar fashion is to reduce transient response, increase coupling and reduce size and cost.

Note that the above design method for the transformer only considers one half of the primary at a time. If the collector to collector impedance is desired to be known (more usual) then multiply  $R_{L21}$  by 4 (four). Or the turns ratio is given by:—

$$(N1 + N3) \div N2 = \sqrt{4 R_{L21} \div R_L}$$

Most ready made transformers specify a collector to collector impedance instead of collector to centre tap impedance. In that case use the above equation.

4. The input transformer (T1) turns ratio can be calculated from the following formula with reference to Fig. 11:—

$$N_p \div N_{ss} = \sqrt{r_{ee} \div (4 \times r_{ie})}$$

where  $r_{ee}$  = collector-emitter small signal resistance of driver transistor.

$r_{ie}$  = small signal input resistance of the output transistor.

$N_p$  = Number of turns on primary.

$N_{ss}$  = Total base-to-base (c.t.) turns on secondary.

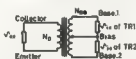


FIG. 11.

The values of  $r_{ee}$  and  $r_{ie}$  can be found as in the single ended stage method for either  $T_{s1}$  or  $T_{s2}$ .

5. For push-pull operation the power input required to drive the amplifier is found from

$$P_i = 3 \times V_{os} \times I_{s1}$$

Design your driver accordingly.

Well, that completes a simple (?) approach to the design of class A power amplifiers. Unfortunately I had to limit the design cases and have not included complementary symmetry or transformerless amplifiers as I considered these special cases that did not have wide applications in Amateur Radio.

One thing I have not considered above is the stabilisation of base current against large temperature changes. This will be included under class B design—which will include a discussion on heat sinks.

The above data applies to PNP as well as NPN transistors—all you have to do is use the right symbols in the circuit and the right battery polarity. Any queries should be addressed to me including an s.a.e.

#### REFERENCES

- "Transistor Circuit Design," Texas Instruments.
- "Transistor A.F. Amplifiers," Jones and Hillbourne.
- "Transistor Physics and Circuits," Riddle and Rutenbatt.
- "Principles of Transistor Circuits," R. F. Shea.
- "73 Magazine."

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# SIDEBAND

Sub-Editor: PHIL WILLIAMS, VK6N

## S.S.B. IN THE R.D. CONTEST

This month I must comment on the obvious increase in s.s.b. operation during the Remembrance Day Contest. It is, of course, a fact that most people now operate throughout the contest with the c.w./s.s.b. detector with b.f.o. in the "on" position and tune all the a.m. stations as single sideband signals. The high scorers, such as VK2AHM, use a.m. transmission so that they can collect up all of the stations which appear on the band. Those like myself, who do not possess a.m. gear (except on 142 mcs.) are prepared to miss out those a.m. stations which are either too badly frequency modulated or "pulled," or which are not equipped with b.f.o.'s, or whose ancient procedures are too long-winded for contest operation.

One instance which comes to mind was when four sideband stations were all on frequency for a "fresh" a.m. station which had just opened up on the 80 metre band on Saturday evening. After a few minutes of calling, in turn and without mutual interference, they all agreed to seek pastures new as the a.m. man did not answer, did not comment, but just went on calling CQ with no a.m. replies, even. I am sure the sidebanders have absolutely no complaint about the a.m. stations which were correctly operated except perhaps for the occasional loud heterodynes from the carriers.

This year I operated for about 14 hours for 291 contacts, about 29% of which were a.m. and the rest sideband. This indicates the trend towards s.s.b., and the improved operating procedures which have accompanied its introduction. Even in the so-called "dog-piles" it was possible to sort out who was in there about third layer down, without the clobbering of the carriers—which, of course, blot out everything, with the result that everybody has to start all over again.

It was a wonderful contest and gets better every year—but where were the VK2s this year?

## CERAMIC FILTERS FOR S.S.B.

A recent article in the R.S.G.B. "Bulletin" for July 1966 describes a transistor s.s.b. exciter using a ceramic disc filter with characteristics at the 6/60 db. points similar to the popular mechanical filters from U.S.A. and Japan. The particular filter used is a Brush-Clerite filter type TL-2D5A, which uses 17 ceramic disc elements arranged in a very compact filter as shown in Fig. 1. This ingenious filter is compatible with transistor equipment as far as both size and imped-

application of these for receivers for elimination of strong signals on adjacent channels. Other advantages of the ceramic filters are their robustness, stability, low pass-band ripple (1 to 3 db. when correctly terminated) and wide range of operating temperature ( $-40^{\circ}\text{C}.$  to  $+85^{\circ}\text{C}.$ ). Before anybody gets too excited about such performance, it must be stated that the price in Australia is likely to be just in excess of that of a mechanical filter (several dollars more).

So far I have been unable to find out whether carrier crystals for the oscillators are available to suit the filters, but these of course would cost extra, and would need to be specially selected.

Although I have not had an opportunity to test these filters as none, to my knowledge, have been imported yet, but my "G" sources tell me they are absolutely ideal for transistor receivers, being about the size of an inch and a half of the end of your "Biro"

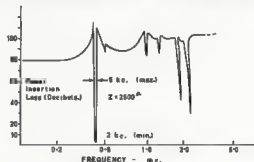


FIG. 2. Approx. Wide band response of Ceramic filter type TL2D5A. (17 Element)

ance are concerned, as its input and output impedances are both 2500 ohms, and it requires no coils or tuning capacitors, so that connection directly to the circuits is practicable.

The wide-band response curve shown in Fig. 2 indicates some quite remote spurious responses which are easily removed by simple L.I. transformers of the type used in 455 Kc. circuits in receivers. A good feature of these filters is the high attenuation just outside of the passband, which settles down at better than 70 db. below the level of the frequencies within the band. Sidebanders will appreciate the

pen. About 80 db. of stop band attenuation in one-tenth of a cubic inch is quite an achievement.

Where these filters are to be used with valve circuits, the use of L or Pi matching circuits to increase the input and output impedances, is normal practice.

Published data states that the linearity of the phase-shift throughout most of the pass-band is adequate for most applications, and speech quality in the exciter described in the R.S.G.B. article was stated to be excellent.

Vibration and shock tests as per MIL-STD-202B, were stated to be mild for this type of filter, and extreme tests indicated that G-forces in excess of 100 were necessary to cause intermittent performance, and the filter returned to within tolerance after the test.

This data is published for pure interest for readers as these filters are relatively new and could offer a new avenue for experiment. I should be interested to pass on information from anybody who has had practical experience with them.

73 for now, Phil 5NN.

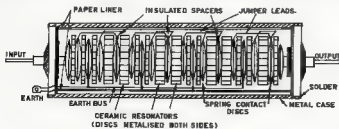


FIG. 1. CERAMIC LADDER FILTER - 17 ELEMENT.

(Approx.  $1\frac{1}{2}$ " Long x  $\frac{3}{8}$ " Dia.)

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### SPECIFICATIONS

FREQUENCY RANGE: 3775-4025 kc, 7050-7300 kc, 14.1-14.35 mc, 21.20-21.45 mc. TUBE AND SEMICONDUCTOR COMPLEMENT: 2—6GB5 power amplifier, 1—12DQ7 driver, 23—transistors, 18—diodes, 1—zener diode, 1—Varactor diode. SIZE: 5"H, 11 1/2"W, 10"D. Shipping weight, Approx. 20 pounds.

TRANSMITTER POWER INPUT: 135 watts. (Slightly lower on 15) DISTORTION PRODUCTS: Down at least 25 db CARRIER SUPPRESSION—50 db. SIDEBAND SELECTION: Upper or lower sideband selectable by panel switch. UNWANTED SIDEBAND: Down 40 db min @ 300 cps. ANTENNA IMPEDANCE: 40-100 ohms unbal. AUDIO BANDSWITCH: 300-2400 cps @ 6 db.

### RECEIVER

SENSITIVITY: 1  $\mu$ V for 10 db signal/noise. SELECTIVITY: 2.1 kc @ 6 db, 5.3 kc @ 60 db. SPURIOUS RESPONSE: Images and IF response down at least 40 db. STABILITY: Less than 100 cps drift in any 30 minute period under any normal ambient condition. AUDIO OUTPUT: 2.0 watts @ 10% distortion. TUNING RATE: 14 kc per revolution (slow) 80 kc per revolution (fast). SPEAKER: 3.2 ohms built-in. Terminals on rear for external speaker. POWER SUPPLY: Built-in 117V AC/12V DC (negative ground) dual supply. Conversion is made automatically by proper line cord.

### POWER CONSUMPTION

AC OPERATION: 35 watts, receive 165 watts transmit (single tone). DC OPERATION: 0.5A receive only (Standby) 3.6A receive (xmtr ready) 16.0A transmit (single tone).

### ACCESSORIES

● Model SB-2, VOX ● Model SB-2XC, 100 kc crystal calibrator ● Model SB1-MB mounting plate for mobile use ● Model SB-1MIC controlled magnetic microphone ● SB1-LA LINEAR AMPLIFIER. Operates at 1,000 P.E.P. input on 80, 40 and 20 meters, 750 watts on 15 meters. Size: 5 1/2"H x 11 1/2"W x 11 1/2"D.

SINGLE SIDEBAND communications on four popular amateur radio bands (80, 40, 20 & 15 meters) are offered in a new transistorized transceiver from Sideband Engineers, a unit of Raytheon Company. Compact, 20-pound SB-34 measures only 11 1/2" by 10" by 5" and can be operated as a base station or a mobile unit from either 117 volt AC or 12 volt DC from SBE.

A COMPLETELY NEW SIDEBAND TRANSCEIVER, SB-34! All of the design features introduced originally in the SB-33, and now well proved have been retained... an entirely new series of "plus performance" features have been added. And SB-34 is handsome equipment... conservatively styled, attractively appointed... is in a physical "package" that is even smaller than SB-33! Feature-wise... dollar-wise... SB-34 LEADS THE FIELD... represents the biggest transceiver value EVER! Here are some of the reasons:

### SB-34 HAS A BUILT-IN UNIVERSAL

POWER SUPPLY! Just connect the equipment directly to the vehicle 12 volt battery using the cable provided! Or use the second cable and plug it into 117 volt AC power supply. No inverters or other supplementary equipment needed.

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Drain-saving panel switch turns off transmitter tube filaments and power supply for casual listening. In this condition, SB-34 draws only 1 ampere from the car battery!

UPPER OR LOWER SIDEBANDS ARE SELECTABLE BY PANEL SWITCH. The two sidebands are locked positively to the carrier—dial shift can't occur.

### LOUDSPEAKER IS BUILT-IN.

A COLLINS MECHANICAL FILTER is used both on transmit and receive; gives exceptional selectivity and a clean, sharp transmitted signal.

EXPANDED FREQUENCY COVERAGE. SB-34 provides 250 kc on 80-40-20-15 meter bands, covers MARS and out-of-band DX frequencies. (See specifications for specific ranges.)

SOLID-STATE SWITCHING... NO RELAYS IN SB-34, all circuits are switched from receive to transmit by modern solid-state techniques—no break-through in transceiver design that eliminates all relays!

### SOLID-STATE, ALC CONTROL.

SOLID-STATE DIAL CALIBRATION: EXCLUSIVE Varactor circuitry and control allows easy dial calibration to operating frequencies. SB-34 has provision for 100 kc crystal calibrator, includes calibrator ON-OFF front panel switch.

DELTA RECEIVER TUNING. With this feature receiver can be tuned over a range of several kilocycles either side of the transmitter frequency. This eliminates the "leap frogging" problem.

LOW FREQUENCY DRIFT... Drift is normally less than 100 cycles in any 30 minute period under normal ambient conditions.

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Transistor Amplifier Design

AUTHOR'S REPLY

Editor "A.R." Dear Sir,  
I feel obliged to defend myself in the face of Mr Metzenthens criticisms as I feel some misunderstanding has occurred. I will answer his points as he presented them

1. Somehow this did not appear in the article—it is in my notes, but I think that, as some knowledge of transistors is assumed, then people who choose to use a high supply voltage would check this anyway

2. My choice of  $I_C$  was made to cover the general case. I will admit that out of approximately 180 transistor characteristics I perused, I found three that had their highest  $h_{FE}$  just below 2 mA. They were: SE4010, 2N3839, and 2N3840.

I found that  $h_{FE}$  was, in most cases, best between 3 and 5 mA.

I do not agree that silicon transistors can usually be operated with a very low  $I_C$  except where gain is of secondary importance and/or a higher input impedance desirable.

3. Quite true—but the equation

$$R_C = \frac{V_{CC}}{I_C} \dots \dots \dots (1)$$

was taken from the half voltage rule which states

$$V_{CE} \text{ is less than or equal to } \frac{V_{CC}}{2} \dots (2)$$

Now, for thermal stability we must have an emitter resistor, the voltage drop ( $V_{BE}$ ) across which cannot be ignored—thus

$$V_{CE} < \frac{V_{CC}}{2} \dots \dots \dots (3)$$

for these circumstances.

So as to provide people with a starting point, I said let

$$V_{CE} = \frac{1}{2} V_{CC} \dots \dots \dots (4)$$

as this fulfils the above condition in equation (3). When all worked out,  $V_{CE}$  will not equal  $V_{CC} + 3$ .  $V_{BE}$  will be less than  $V_{CC} + 3$  and consequently  $V_{CE}$  will approach  $V_{CC} + Z$ , thus making equation (1) valid.

It is next to impossible to say what the final value of  $V_{CE}$  is beforehand. I chose to let  $V_{CE} = V_{CC} + 3 \dots (4)$  to enable  $R_E$  and  $R_C$  to be calculated and provide a starting point that would not upset the final value of  $I_C$  by a significant amount. For further information see "Reference Manual of Transistor Circuits" by Mullard; "Germanium and Silicon Transistors and Diodes" by Philips; and the "Transistor Manual" by G.E.

4. Arguments on the correctness of this equation could cause a major controversy. I have seen a derivation of this equation which, to me, appears reasonable. Mr. Peter Hammer (VK-3ZPI) kindly supplied me with his version of the correct equation plus a derivation. Mr. Metzenthens has failed to supply me with what he thinks the correct equation is and a derivation (which, I think under the circumstances, is needed). I wonder if we all end up with separate equations?

I feel though that I should defend my use of this equation and answer Mr. Metzenthens' criticism.

- (a) It is not a printer's error.
- (b) Prior to publication, and despite much research, I found no other equations.
- (c) Upon investigation it appeared to work satisfactorily.

5. I think these assumptions are quite reasonable for the following reasons:—

(a) Considering the wide variations in  $R_{in}$ , I had to fix upon some value that would give reasonable results (i.e. nothing drastic would occur). For germanium transistors the value of  $R_{in} = 500$  ohms was chosen to suit many situations—I will admit it is on the low side as is the value for silicon transistors.

(b) The values are chosen this low to give errors that are on the high capacitance side which, I think, is the desirable side.

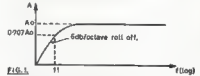
(c) For most cheap, low level application, silicon transistors (i.e. ones that are most likely to be used), the range of  $R_{in}$  is between 480 and 1400 ohms (roughly). Is not 1000 ohms a reasonable average? (For further reference, see "Transistors" by Dwyer, and "Transistor Manual" by G.E.)

6. Here I shall concede that I made a genuine blunder—sorry. It should read 1300 ohms. I made a mistake in transcribing some information from a piece of paper to my notes. This type of error is hard to pick up when you have innumerable things to consider simultaneously (ever tried to write an article?).

It should be understood that the example serves just to illustrate the method—nevertheless, it should be correct and I apologise for my error.

7. I hope Fig. 1 clarifies the situation.

I did consider including this in the article but when I came to condense my notes I decided that it was unnecessary and would be reasonably clear from the later example.



Anyhow, the equations (1) and (2) were only included so that people who found that the graphs did not fit their circumstances could calculate an appropriate value for  $C_E$  and  $C_C$ .

I shall ignore his last comment.

In conclusion, I would like to add that Mr. Metzenthens seems to have lost sight of the fact that the article was not an engineering approach to the subject.

It was written for the home constructor who—

- (a) Cannot find a circuit to suit his needs;
- (b) Wants to use a transistor on hand, or just wants to use a transistor;
- (c) Does not just want to "lift" a circuit from elsewhere, or

(d) Does not wish to involve himself in lengthy theoretical considerations which he may not understand.

Despite the fact that the equation for  $C_E$  is in dispute and assumptions were made for the values of  $R_{in}$ , the system works and nothing catastrophic will result from its use.

—Roger L. Harrison, VK3ZRY.

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New South Wales:		miles
52 Mc VK4EAD to VRTAQQ, 8/4/58		750
144 Mc VK2ZMR to ZL3AAZ, 8/1/58		1410
432 Mc VIVP/1 to VK2EPT, 14/8/58		176
578 Mc No claim		
1386 Mc VK2EAC to VK2ZCF/R, 4/3/58		468
Victoria:		
50 Mc VK3ALZ to XRLFP, 1/8/58		8418
144 Mc VK2ENC to ZL8HP, 13/12/58		2072
432 Mc VK3ALZ to VK2ZDR, 30/3/58		486
578 Mc VK3AKE to VK3ANW, 11/12/49		80.7
1206 Mc VK3ALZ to VK3AUX/5, 10/4/58		26.5
2306 Mc VK3EAC to VK3ANW, 15/3/58		9.4
3306 Mc VK2ZQT/ZGX/5 to VK2ZDQ/5, 14/12/53		9.4
Queensland:		
50 Mc VK4AZZ to KERRG, 16/3/58		3905
144 Mc VK4ZWB to VK1ZAO/TZAO, 8/1/58		1117
No other claims		
South Australia:		
50 Mc VK3KL to WIACS/KH5, 26/8/47		3361
144 Mc VK3ZJH to VK3ZCN, 8/1/58		1330
432 Mc VK3ZDR to VK3ALZ, 30/3/58		486
578 Mc VK2YM/Z2P/5 to VK3ZIS/5, 22/11/55		105.3
1215 Mc VK3AA/5 to VK5ZCR/5 (now VK5SK), 6/1/53		1.0
Western Australia:		
50 Mc VK8BE to JASBP, 30/10/58		5490
144 Mc VK3ZCN to VK3ZJH, 8/1/58		1330
432 Mc VK5ZDS to VK3LK/5, 25/4/58		66.5
578 Mc VK5ZDS to VK3LK/5, 15/12/53		101.3
No claims		
Tasmania:		
50 Mc VK7LZ to JASBL, 3/12/58		2443
144 Mc VK1ZAO/TZAO to VK4ZWB, 8/1/58		1117
432 Mc VK1ZAO to VK5ZDM, 8/1/58		913
N.B.—Australian Records in bold type.		

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13/16 in.	\$3.90	2-1/8 in.	\$8.60
7/8 in.	\$4.00	2-3/16 in.	\$8.60
1 in.	\$3.90	2-1/4 in.	\$9.00
1-1/16 in.	\$4.00	2-5/16 in.	\$9.80
1-1/8 in.	\$4.00	2-3/8 in.	\$10.40
1-3/16 in.	\$8.00	2-1/2 in.	\$11.00
1-1/4 in.	\$5.20	2-3/4 in.	\$12.40
1-1/2 in.	\$5.80	2 1/2 in.	\$12.40
1-3/8 in.	\$5.60	3-1/4 in.	\$13.80
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**Type K5B20:** Normal a.c. (r.m.s.)  
Circuit Voltage, 240 r.m.s., Cur- \$3.45 + S.T. 12½%  
rent capacity 5 amps.

Pulse Diode, Type K2C .... 78c plus S.T. 12½%  
Pulse Transformer .... \$1.20 plus S.T. 12½%  
Please add packing and post, 10c Set.

NOTE: A Circuit is available for making a 1,000 watt Light Dimmer using K5B20, K2C, Pulse Transformer and a few Resistors and Condensers. Write or call for a copy.

## SILICON DIODES

IN3491—18 amps. at 50 p.i.v.  
Available with either K or A to case, 75c, plus S.T. 12½%  
Heat Sink Adaptors to suit, 25c, plus S.T. 12½%.

S10AR2—1 amp. at 1,000 p.i.v.	\$1.20 plus S.T. 12½%
S15AR2—1 amp. at 1,500 p.i.v.	\$2.00 " "
IN3193 750 mA. at 200 p.i.v.	40c " "
IN3194 750 mA. at 400 p.i.v.	55c " "
IN3195 750 mA. at 600 p.i.v.	75c " "

## LOUDSPEAKERS 4"

Available 3.5, 8 or 15 ohm impedance.  
\$1.50 + 25% S.T.

## TANTALUM CAPACITORS

Available from Stock.

SOLID, SMALL-READ TYPE, RESIN		DIPPED.
50 uF.	3 v.w. Size 8.1 mm. x 5.6 mm.	46c each
40 uF.	3 v.w. Size 8.1 mm. x 5.6 mm.	46c "
30 uF.	3 v.w. Size 7.5 mm. x 4.9 mm.	46c "
20 uF.	6 v.w. Size 8.1 mm. x 5.6 mm.	46c "
15 uF.	10 v.w. Size 8.1 mm. x 5.6 mm.	46c "
10 uF.	15 v.w. Size 8.1 mm. x 5.6 mm.	46c "
7 uF.	20 v.w. Size 8.1 mm. x 5.6 mm.	46c "
5 uF.	25 v.w. Size 8.1 mm. x 5.6 mm.	46c "
4 uF.	35 v.w. Size 8.1 mm. x 5.6 mm.	46c "
3 uF.	35 v.w. Size 7.6 mm. x 4.9 mm.	46c "
2 uF.	35 v.w. Size 7.6 mm. x 4.9 mm.	46c "
1.5 uF.	35 v.w. Size 6.6 mm. x 4.1 mm.	46c "
1.0 uF.	35 b.w. Size 6.6 mm. x 4.1 mm.	46c "
.7 uF.	35 v.w. Size 6.1 mm. x 3.6 mm.	46c "
.5 uF.	35 v.w. Size 6.1 mm. x 3.6 mm.	46c "
.4 uF.	35 v.w. Size 6.1 mm. x 3.6 mm.	46c "
.3 uF.	35 v.w. Size 6.1 mm. x 3.6 mm.	46c "
.2 uF.	3 v.w. Size 6.1 mm. x 3.6 mm.	46c "
.15 uF.	3 v.w. Size 6.1 mm. x 3.6 mm.	46c "
.1 uF.	3 v.w. Size 6.1 mm. x 3.6 mm.	46c "

Above prices are plus Sales Tax 25%.

## TRANSCIVERS

Three transistors. Range up to ½ mile, depending on terrain. Supplied complete ready for use with telescopic antenna and batteries.

**\$17.35 Set of Two + 12½% S.T.**

Also 5-transistor model.  
**\$23.50 Set of Two + 12½% S.T.**

And 9-transistor model.  
**\$53.85 Set of Two + 12½% S.T.**

## BELPHONE INTERCOMM. SYSTEMS

Comprises two handsets (similar P.M.G. telephone) and connecting wire. Very clear reproduction. Loud bell to call.

**\$8.65 Set (inc. batteries) + 12½% S.T.**

## NEW! MINIATURE POWER SUPPLY

6, 9, 12 volts at 500 mA. Useful for transistor equipment such as tape recorders, record players, radio-grams, etc. May also be used as trickle charger for car batteries.

**\$10 + 12½% S.T.**



# WARBURTON FRANKI

220 PARK ST. SOUTH MELB., VIC. PHONE 30 lines 69-0151



OPEN SAT.  
MORNING

Please include  
postage or  
freight with  
all orders



# ROSS HULL MEMORIAL V.H.F. CONTEST, 1966-67

The Federal Contest Committee of the Wireless Institute of Australia invites all Australian and Overseas Amateurs and Short Wave Listeners to participate in this annual contest which is held to perpetuate the memory of Ross Hull whose interest in v.h.f./u.h.f. did much to advance the art.

A Perpetual Trophy is awarded annually for competition between members of the W.I.A. in Australia and its Territories, inscribed with the name and life work of the man whom it honours. The name of the winning member of the W.I.A. each year is also inscribed on the Trophy. In addition, this member will receive a suitably inscribed certificate.

**Objects:** Australian Amateurs will endeavour to contact as many other Amateurs in Australia and Overseas under the following conditions.

**Date of Contest:** From 0001 hrs. E.A.S.T., 10th December, 1966, to 2359 hrs. E.A.S.T., 15th January, 1967.

**Duration:** Any seven calendar days within the dates mentioned above, not necessarily consecutive. These periods are to be at the operator's convenience. A calendar day is from 0001 hrs. E.A.S.T. to 2359 hrs. E.A.S.T.

## RULES

1. There are two divisions, one of 48 hours duration, and one of 7 days. In the 7-day division, there are three sections:—

- (a) Transmitting, Open;
- (b) Transmitting, Phone;
- (c) Receiving, Open.

2. All Australian and Overseas Amateurs may enter for the Contest whether their stations are fixed, portable or mobile.

3. All Amateur v.h.f./u.h.f. bands may be used, but no crossband operating is permitted. Operators are cautioned against operating transmitting equipment on more than one frequency at a time, particularly when passing cyphers. Crossband operation to assist contest working is prohibited.

Such operation will be grounds for disqualification. Cross mode contacts will be permitted.

4. Amateurs may enter for any of the transmitting sections. The seven-day winner is not eligible for the 48-hour award.

5. Only one contact per band per station is allowed each calendar day.

6. Only one licensed Amateur is permitted to operate any one station under the owner's call sign. Should two or more operate any particular sta-

tion, each will be considered a contestant and must submit a separate log under his own call sign.

7. Entrants must operate within the terms of their licenses.

8. **Cyphers:** Before points may be claimed for a contact, serial numbers must be exchanged. The serial numbers of 5 or 6 figures will be made up of the RS (telephony) or RST (c.w.) report plus three figures commencing from 001 for the first contact and will increase in value by one for each successive contact. If any contestant reaches 999, he will start again with 001.

9. **Entries** must be set out as shown in the example, using only one side of the paper. Entries must be postmarked not later than the 13th February, 1967, and clearly marked "Ross Hull Contest," and addressed to **Federal Contest Manager, Box N1000, G.P.O. Perth, W.A.**

## SCORING TABLE

Distance in Miles	33 Mc.	144 Mc.	432 Mc.	576 Mc.	Higher
Up to 25 miles	1	1	2	10	20
26 to 50 "	1	1	10	25	50
51 to 100 "	2	5	25	75	100
101-200 "	5	10	50	100	200
201-300 "	15	15	75	200	
301-500 "	10	20	100		
501-1000 "	5	25	200		
1001-1500 "	10	50			
1501-2500 "	20	100			
2501-3500 "	35	200			
3501-5000 "	50				
5001-8000 "	100				
8001 and over	200				

10. **Scoring** for all sections will be based on the attached table. Distances must be shown in the log entry as shown in the example. Failure to make this entry will invalidate the particular claim. Some typical distances are given in the attached table.

11. **Logs:** All logs shall be set out as in the example and addition will carry a summary sheet showing the following information:

Name ..... Call Sign  
Address ..... Division  
..... Claimed Score  
Operating Dates ..... (7 cal. days)

Highest score over a 48-hour period was ..... points.

Operating period:  
from ..... hrs. E.A.S.T. .... /5 -  
to ..... hrs. E.A.S.T. .... /5 -

**Declaration:** I hereby certify that I have operated in accordance with the conditions of my licence and abided by the Rules of the Contest.  
Signed \_\_\_\_\_

Date \_\_\_\_\_

12. Entrants not abiding by the Rules of this Contest will be disqualified.

13. The ruling of the Federal Contest Committee of the W.I.A. will be final. No dispute will be entered into.

14. **Awards:** Certificates will be awarded to the winners of each section in each VK and Overseas Call Area. The VK contestant who returns the highest score in the transmitting section and who is a financial member of the W.I.A. will have his name inscribed on the Trophy which will be held by his Division for the prescribed period. A certificate will be awarded to the contestant, who shall not be the Trophy winner, and who returns the highest scoring log covering a period of any 48 consecutive hours. Also, certificates will be awarded for operating in the Ross Hull Contest and breaking any Australian v.h.f./u.h.f. distance record.  
The Distance Table for scoring is shown on Page 12.

## RECEIVING SECTION

1. Short Wave Listeners in Australia and Overseas may enter for the Contest, but no active transmitting station may enter.

2. Contest times and logging of stations on each band are as for the transmitting sections, however there is no 48-hour sub-section.

3. To count for points, logs will take the same form as for transmitting sections, but will omit the serial number received. Logs must show the call sign of the station heard (not the station worked), the serial number sent by it, and the call sign of the station being worked.

Scoring will be on the same basis as for transmitting stations, i.e. on the distance between the listener's station and the station heard. See the examples given. It is not sufficient to log a station calling CQ.

4. A station heard may be logged only once per calendar day on each band for scoring purposes.

5. **Awards:** Certificates will be awarded to the highest scorer in VK and Overseas countries.

## EXAMPLE OF TRANSMITTING LOG (Brisbane Station)

Date/ Time E.A.S.T.	Band Mc.	Emission Power	Call Sign	RST/No. Sent	RST/No. Rcvd.	Dist. Miles	Points Claim
9th Dec. 9100	82	A3 (a)	VK7ZAI	58001	38004	1110	18
E.A.S.T. 9110	82	A3 (a)	VKING	58008	57051	320	10
E.A.S.T. 9230	144	A3	VK5ZK	56005	35043	890	25
E.A.S.T. 9235	144	A3	VK3ZJQ	45004	46021	850	25

## EXAMPLE OF RECEIVING LOG (Perth S.w.I.)

Date/ Time E.A.S.T.	Band Mc.	Call Heard	RST/No. Sent	Station Called	Distance Miles	Points Claim
2nd Jan 1000	82	VK5ZDK	56221	VK3KXK	1330	10
E.A.S.T. 1005	82	VK3ZCF	58185	VK5ZAA	2040	10
E.A.S.T. 1110	432	VK6ZDS/S	57061	VK6LX/S	80	25
E.A.S.T. 3rd Jan 6500	144	VK3ZJQ	44102	VK5ZCN	1330	20

# 1966 R.D. CONTEST RESULTS

## VK6 FOR '66

The Federal Contest Committee announces the results of the 1966 R.D. Contest. VK6 wins by a narrow margin from VK5, who have held this position for the past two years.

Allowing for cross-mode operation, the States' scores are higher than previous years. This is due to enthusiastic participants making better use of their time.

The logs this year were of a higher standard and operators are complimented for their prompt despatch of their logs, enabling an early announcement of the results.

Next year's rules will include Z call licenses and the scoring principle as suggested by the Federal Communications Manager.

—Neil Penfold, VK6ZDK, for F.C.C.

### DETAILS OF STATE SCORES

State	Log Entry	Licences	%	Total Score	Aver. Top Six Logs	State Points
New South Wales	100	1,296	7.7	19,286	778	2,264
Victoria	74	1,101	6.7	21,619	897	3,239
Queensland	90	444	20.3	18,510	996	4,754
South Australia	97	474	20.5	20,539	832	5,043
Western Australia	74	266	27.8	15,405	944	5,228
Tasmania	39	128	30.5	8,093	840	3,108

### STATE TROPHY WINNER

#### Western Australia

#### STATE PLACINGS

Western Australia	1
South Australia	2
Queensland	3
Victoria	4
Tasmania	5
New South Wales	6

### AWARD WINNERS

#### Phone—

VK1QL	810	VK6RY	990
2KA	675	7TX	873
3MO	1273	8DI	173
4BQ	1018	9DJ	1539
5EF	918		

#### C.W.—

VK2QL	493	VK6WT	392
3AXK	481	7GK	352
4XW	903	8HA	273
5FO	365	8CJ	165

#### Open—

VK1DA	453	VK6RU	990
2AHM	1304	7SM	1290
3AKS	693	7AG	328
4RH	1369	8MI	990
5BI	588		

#### Section D—Receiving

VK1—J. Hurren	375 pts.
VK2—A. Nutley	1083
VK3—P. Forbes	784
VK4—D. Clark, L4144	1042
VK5—J. Ross	917
VK6—F. Price, L6003	875
VK7—G. C. Johnston	1305
Club Entry—Vic. Amateur Listeners' DX Club	954

#### Section E—V.h.f./U.h.f.

VK2ZCF	84	VK5ZDX	53
3ZCK	60	6ZER	6
4ZEP	8	7ZJG	26

### AUST. CAPITAL TERRITORY

#### Top Six Logs—

VK1QL	416 pts.	VK1DA	423 pts.
1VP	299	1JL	313
1VK	218	1JG	285

#### Phone—

VK1QL	610 pts.	VK1L	296 pts.
1VP	299	1TY	188
1JG	313	1GB	80

#### Open—

VK1DA	439 pts.	VK1PI	68 pts.
1VK	410		

### NEW SOUTH WALES

#### Top Six Logs—

VK1AHM	1384 pts.	VK1ROP	644 pts.
1BO	888	2AT	573
1XA	678	2ARF	584

#### Phone—

VK1XA	675 pts.	VK1NZ	84 pts.
1BGF	584	2DH	83
2AKF	584	2AKL	83
2PF	470	2ANL	84
2ALY	440	2CU	80
2ABC	390	2BQ	78
2AZO	394	2AIK	78
2APD	438	2CK	71
1BKK	365	2BCE	67
2PK	350	2BQ	65
2ACD	299	2SG	61
2OD	299	2VH	56
2ACF	290	2BU	52
3RU	350	2VH	52
2ARV	235	2APQ	49
2SS	230	2AC	47
2ARZ	217	2BU	47
2HO	180	2BPL	46
2BQ	180	2RL	44
2HW	179	2ABO	44
2AVT	178	2AAH	40
2EK	175	2ADA	40
2ADC	174	2ADI	40
2EB	167	2AKA	38
2XT	157	2XN	37
2ZK	130	2AAJ	34
2AVJ	118	2AKJ	13
2APFA	113	2ABB	12
2TS	111	2BM	11
2ACK	103	2TP	11
2AHP	98	2EH	9

#### C.W.—

VK1QL	483 pts.	VK1EL	106 pts.
2AGH	335	2ZC	147
2TS	306	2PQ	148
2XQ	296	2AUQ	136
2VH	232	2ATA	118
2ADJ	220	2TV	69
2EO	220	2HZ	61
2WT	217	2AC	47
2TS	216	2AC	32
2GT	194	2AM	12
2GW	171	2AWI	9

VK1AHM	1394 pts.	VK1ML	236 pts.
2RO	898	2AKE	204
2AT	873	2VS	141
2AAR	395	2BCC/P	134
2AGH	348	2HC	80
2PU	330	2IC	66
2SU	288	2AKO	54
	284	2ANL	38

#### Open—

VK1AHM	1394 pts.	VK1ML	236 pts.
2RO	898	2AKE	204
2AT	873	2VS	141
2AAR	395	2BCC/P	134
2AGH	348	2HC	80
2PU	330	2IC	66
2SU	288	2AKO	54
	284	2ANL	38

### VICTORIA

#### Top Six Logs—

VK1MO	1373 pts.	VK1SE	789 pts.
3ARD	825	3WK	793
3DF	880	3LW	721

#### Phone—

VK1MO	1373 pts.	VK1NN	214 pts.
3ARD	825	3AKO	150
3DF	880	3AFU	304
3EG	780	3WY	183
3WK	723	3RT	178
3LW	721	3LK	170
3RV	713	3PP	167
3AFU/P	640	3AWV	152
3ADW	619	3AM	148
3CY	537	3PT	138
3AS	489	3AKS	128
3JAN	478	3ATN/P	84
3AGM	376	3ARM	88
3VE	374	3VT	85
3AKK	358	3AEP	83
3SM	339	3ALE	83
3DC	283	3VY	64
3DG	275	3XV	61
3CK	275	3YK	50
3EF	273	3ARJ	38
3DY	239	3BQG	38
3AAO	239	3AAC	28
3ZU	221	3AFJ	19
3AWT	221		

#### C.W.—

VK1AJX	481 pts.	VK1QP	205 pts.
3APJ	423 "	3ARV	148 "
3ADB	300 "	3UM	82 "
3IB	314 "	3AEY	26 "
3RJ	261 "	3ZZ	7 "
3APR	248 "	Check Log 3GB	

#### Open—

VK1AKS	653 pts.	VK1KK	187 pts.
3QV	578	3AHW	115
4XB	433	3KS	118
3ADN	393	3PS	113
3OP	346	3AWM	103
3BR	171	3KB	86
3ABA	160	3AJB	80

### QUEENSLAND

#### Top Six Logs—

VK1RH	1393 pts.	VK1RW	886 pts.
4LT	1089	4AL	870
4BQ	1013	4AK	798

#### Phone—

VK1BQ	1013 pts.	VK1TE	81 pts.
4WV	845	4EH	48
4AL	875	4PK	48
4AK	788	4WL	40
4TM	787	4TP	38
4FA	787	4XN	38
4N	598	4C	38
4NH	598	4QC	38
4MP	478	4ZZ	32
4PS	463	4HD	32
4DO	423	4X/P	31
4KO	423	4FN	30
4CK	381	4JJ	28
4B	381	4WV	28
4MT	387	4CW	35
4DZ	345	4RW	34
4OF	321	4RC	32
4PJ	319	4QF	31
4MY	317	4GT	21
4WV	307	4WV	20
4DV	183	4LA	20
4WV	146	4OR	19
4EQ	131	4GC	17
4RL	97	4AH	14
5CZ	85	4GZ	14
4XY	85	4GZ	14
4LE	85	4SA	13
4XJ	78	4EP	13
4UD	78	4AN	10
4SD	78	4NG	10
4CS	69	4RW	8
4B	69	4B	8
4UB	69	4XB	8
4PX	61	4HZ	8
4BO	61		

#### C.W.—

VK1W	306 pts.	VK1XP	74 pts.
4ZF	228	4UU	18
4UC			

Open—			
VK4RH	1369	VK4AI	134 pts.
4UR	1008	4WV	79
4VX	727	4WO	66
4BZ	653	4YB	28
4DP	448	4VO	13

Open—			
VK6RU	1385	VK6SM	340 pts.
6PH	854	6AV	79
6BE	536	6MA	66
6KK	484	6YA	42
6NS	453	6HP	42

Victoria—			
VK2ZC	80 pts.	VK3AMK	8 pts.
2ZVY	7		
Queensland—			
VK2ZK	8 pts.	VK3RG	3 pts.
2ZMW	7		

## SOUTH AUSTRALIA

Top Six Logs—			
VK3TF	814 pts.	VK6KM	814 pts.
3IZ	81	3EK	778
3NY	843	3GZ	778

Phone—			
VK3TF	814 pts.	VK6KM	75 pts.
3IZ	881	3LH	74
3NY	845	3PJ	67
3KCM	723	3MA	64
3EK	773	3VB	64
3GZ	773	3TU	63
3NN	735	3NW	61
3ZL	693	3YS	49
3NS	583	3CF	48
3OH	541	3DT	45
3CD	501	3EW	45
3GX	497	3ZL	40
3BG	455	3PI	38
3KCM	444	3PH	37
3LN	443	3MM	35
3TY	354	3ZA	35
3TY	354	3PC	34
3CL	334	3CL	33
3PL	318	3CF	30
3SM	298	3VO	29
3LC	297	3PR	29
3WN	270	3WI	25
3JC	233	3DO	23
3WG	230	3JO	23
3XL	213	3OK	23
3MT	185	3ST	17
3ST	187	3DO	13
3BQ	159	3SB	13
3AL	145	3SP	11
3SS	108	3UT	11
3TN	99	3ZK	9
3OB	88	3OF	8

C.W.—			
VK6FO	385 pts.	VK6RX	45 pts.
6CK	284	6ST	43
6LO	197	6RK	32
6OR	137	6PT	32
6GP	99	6BO	30
6TL	81	6JO	29
6AE	61	6KE	18
6KE	50	6SU	8

Open—			
VK6RI	588 pts.	VK6RM	191 pts.
6PF	488	6NR	161
6AX	401	6PH	157
6VO	398	6SO	156
6ZF	314	6CV	115
6AY	290	6EO	101
6ZQ	286	6NK	86
6QR	275		

## WESTERN AUSTRALIA

Top Six Logs—			
VK6RU	1385 pts.	VK6PH	854 pts.
6RX	877	6CW	857
6XX	857	6LA	873

Phone—			
VK6RY	999 pts.	VK6SZ	86 pts.
6XK	887	6BR	80
6CW	867	6LO	79
6LK	873	6HK	79
6XV	850	6FL	67
6IS	438	6VM	64
6NF	428	6KW	64
6VK	445	6VM	64
6DA	428	6DT	59
6WT	415	6MM	59
6LK/P	330	6KO	45
6CT	305	6KK	40
6CN	295	6TR	37
6CT	241	6VF/P	33
6CY	235	6SK	30
6IS	178	6JO	29
6RG	178	6NN	29
6CD	173	6LM	27
6RS	173	6PW	24
6DM	158	6BS	23
6OR	161	6BC	21
6TZ	147	6KH	19
6DT	147	6YL	18
6KJ	143	6W	17
6BA	136	6W	17
6WL	130	6TH	15
6EB	103	6GL	15
6GH	86		

C.W.—			
VK6WT	285 pts.	VK6ZZ	58 pts.
6RS	200	6AJ	26
6WV	111	6WO	24
6WQ	88	6QJ	18
6AS	65	6JK	11

## TASMANIA

Top Six Logs—			
VK7SM	1385 pts.	VK7AL	630 pts.
7DK	873	7ZZ	515
7TX	873	7XL	464

Phone—			
VK7TX	873 pts.	VK7CC	59 pts.
7AI	530	7LY	54
7GL	454	7CT	53
7JF	371	7PA	49
7SP	361	7B	26
7RM	213	7BT	23
7KH	141	7CR	23
7EB	89	7DW	20
7YS	87	7WZ	14
7WH	81	7BQ	13
7CK	80	7EJ	9

C.W.—			
VK7OK	253 pts.	VK7KA	24 pts.
7RY	178	7AB	23
7GV	94	7AB	19
7JB	60	7LL	13
7BJ	50	7CH	9

Open—			
VK7SM	1385 pts.	VK7OM	590 pts.
7DK	873	7TB	72
7ZL	873	7YL	72
7AL	276		

## NORTHERN TERRITORY

Phone—			
VK8DI	113 pts.		
C.W.—			
VK8HA	373 pts.		

## PAPUA-NEW GUINEA AND TERRITORIES

Phone—			
VK8DG	1380 pts.		
C.W.—			
VK8GJ	185 pts.	VK8MV	10 pts.
Open—			
VK8AG	380 pts.	VK8DR	281 pts.
8XI	380		

## ANTARCTICA

Open— VK6MI — 500 pts.

## SECTION E—V.H.F.

New South Wales—			
VK2ZCF	84 pts.	VK2ZWM	14 pts.
2ZK	65	2ZKX	13
2ZPF	36	2ZC	10
2ZRP	34	2ZBM	9
2ZRU	33	2ZMO	8

South Australia—			
VK2ZK	32 pts.	VK2ZKH	19 pts.
2ZDA	31	2ZVW	19
2ZDM	31	2ZV	18
2ZK	24	2ZKH	11
2ZSJ	21	2ZKA	8

Western Australia—			
VK2ZG	28 pts.	VK2ZFR	11 pts.
2ZAS	17	2ZDK	10
2ZTM	17	2ZAH	5

Tasmania—			
VK2ZG	28 pts.	VK2ZFR	11 pts.
2ZAS	17	2ZDK	10
2ZTM	17	2ZAH	5

## RECEIVING SECTION

Australian Capital Territory—			
J. Murray	378 pts.		
L. Whyte	278		
New South Wales—			
A. Nutley	1083 pts.		
J. Richards, L2043	793		
J. Willard, L2074	748		
P. Linley	641		
C. McGrath, L2344	627		
F. Gendley	617		
C. Middleton-Williams, L3019	419		
P. Cairns	133		
Victoria—			
P. Forbes	784 pts.		
E. Trebblecock, L3043	403		
P. Bolly, L3303	404		
A. Cash	73		
Queensland—			
D. Clark, L4144	1043 pts.		
O. Emborsick, L4187	336		
D. Hunter, L405	336		
K. Cunningham	329		
O. Franks, L4019	174		
N. Boxley, L4155	141		
South Australia—			
J. Ross	917 pts.		
A. Batters, L5085	778		
F. Frendrich, L5094	670		
D. Chagg	481		
A. Wege, L5072	328		
R. Edmeades	30		
Western Australia—			
F. Price, L5003	975 pts.		
M. Ryan	871		
G. Allen	765		
B. Prosser, L5058	474		
S. Marvin, L5038	28		
Tasmania—			
G. C. Johnston	1305 pts.		
B. Morgan	940		
S. Mutton, L2031	914		
B. Everett, L2043	523		
T. Cox	435		
D. Verral	390		
G. Kerr, L2138	331		
H. Westerhof	308		
I. Ellings, L2038	153		
Club Station Entries—			
VK3 Vic. Amateur Listening	DX Club	954 pts.	
VK3 S.W.I. Group of Vic.	L3100	166	
VK4LV Leederville C.B.C.		309	

V.h.f. Contest Distance Table. See Page 17 for Rules.

DISTANCE TABLE										
	Syd.	Canb.	Bris.	Melb.	Hob.	Adel.	N. Zea.	Dar.	Perth	
Sydney .....	0	160	460	460	660	710	1300/	1950	2040	
							1500			
Canberra .....	160	0	600	290	530	670	1300/	1930	1940	
							1500			
Brisbane .....	460	600	0	860	1110	990	1500/	1790	2240	
							1700			
Melbourne .....	460	290	860	0	400	400	1500/	1930	1720	
							1700			
Hobart .....	660	530	1110	400	0	710	1300/	2290	1890	
							1500			
Adelaide .....	710	670	990	400	710	0	1900/	1820	1830	
							2100			
New Zealand	1300/	1300/	1500/	1500/	1300/	1900/	0	2550	3000/	
	1500	1500	1700	1700	1500	2100			3200	
Darwin .....	1950	1930	1790	1930	2280	1620	2550	0	1650	
Perth .....	2040	1940	2240	1720	1890	1330	3000/	1850	0	
							3200			



DF-2

## FOSTER DYNAMIC MICROPHONES FOR HAND-DESK USE

### SPECIFICATIONS:

Output Impedance	50 ohms or 50K ohms
Effective output level	—55 db. [0 db. — (one) 1V. Microbar]
Frequency response	200 to 10,000 c.p.s.

### OMNI-DIRECTIONAL DYNAMIC:

SIZE: 3" x 2-1/8" x 1".  
 Cable: 12 ft. of P.V.C.  
 Switch: on-off.  
 Desk Stand. Clip folds for hand use  
 Colour: WHITE.  
 Plastic Diaphragm.

Retail Price  
**50K ohms**  
**£2/14/0**  
 + Sales Tax 4/9

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*The Standard Manual of Amateur Radio Communication*

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NOW AVAILABLE—

## ★ The Radio Transistor Handbook

by Stoner & Earnshaw.

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# Correspondence

Any opinion expressed under this heading is the individual opinion of the writer and does not necessarily coincide with that of the publishers.

## HISTORY OF EARLY DAYS

Microscope Department,  
University of Queensland,  
George St, Brisbane.

Editor "A.R." Dear Sir,  
I am very interested in obtaining the history of our early pioneer Hans and particularly with respect to the early days of Queensland.

I have endeavored to seek the knowledge myself and it was suggested that I might possibly be more expedient to write to you. I would be grateful for any information you could make available or for further sources of reference.

If you are unable to assist me, could you pass my request to the Federal Secretary of the I.R.U.

Looking forward to your reply.  
Yrs, A. M. SIMPSON,  
Head, Microscope Department.

## SCATHING CONDEMNATION

Editor "A.R." Dear Sir,  
It was with regret that I read in the "A.R.", October, 1966, the scathing condemnation by W. Mettenben of the article by R. L. Harrison on Transistor Amps. Pt. 1.

I feel that Mr. Harrison is to be congratulated on his initiative in preparing this article and assure him that his efforts are greatly appreciated by many.

Mr. Mettenben wishes to air his superior knowledge I would suggest that it might be more palatable in the form of a constructive article rather than a scathing criticism.

—John Paul Hayden VK2BV.

## C.W. WOODDOW

Editor "A.R." Dear Sir,  
Re Federal Comment, "A.R." September, 1966, the scathing condemnation by W. Mettenben of the article by R. L. Harrison on Transistor Amps. Pt. 1.

Key an audio oscillator, with headphone earphone on one ear only.

Have persons in room talk to you on any subject and you reply while you are sending off a newspaper, etc.

—W. N. Short, VK1AAR.

P.S. Unfortunately I had learnt the code in 1930 by the dot and dash, when I was able to join the W.L.A. classes in Sydney in 1947.

At 10.15 p.m. until the above method was used.—BUI.

## GOVERNMENT SUBSIDY

Editor "A.R." Dear Sir,  
For many years the Federal Government has subsidised the rifle club movement throughout Australia on the grounds that rifle shooting is a sport has some defence value in the event of war. It seems to me that the Amateur Radio movement has an equally valid claim for receiving Federal subsidy, especially when one considers the noteworthy contribution made by Amateur Radio operators in the last war.

In the event of such a subsidy being granted, there may be some conditions specified by the Government agencies concerned, but I cannot conceive any situation whereby such conditions could adversely affect Amateur operations.

It seems to me that we have ample grounds for claiming a per capita subsidy for each successful A.O.C.F. or A.O.L.C.F. candidate trained by W.L.A. agencies—by our evening classes, by our correspondence courses and, perhaps, by the Youth Radio Scheme.

Any moneys received on this basis could be applied to the improvement of our training facilities rather than to general W.L.A. administration. In any case, the approval for such a subsidy would give the Institute a status at Government level which it lacks at present and would add weight to any further representations made on other matters at Federal level.

I submit that this is a matter well worth consideration by Federal Executive.

—Rex Black, VK3FA.

## MACQUARIE ISLAND

14 Brockley Street,  
Sale, Vic.

Editor "A.R." Dear Sir,  
I will be going down with this coming year's Antarctic Expedition to Macquarie Island, leaving Australia at the beginning of December.

It has been suggested to me that someone may be interested in leasing me 6 and possibly 2 meters gear for the duration of 1967. I would be willing to set up a v.h.f. station to attempt to communicate with Australia, rare DX and all that I haven't any workable m gear, but hope to obtain some gear all care 6 metre gear during the year, time permitting.

Should anyone be interested in supplying some gear, I would stipulate the following: (1) That the gear be reasonably high power a.m. i.e. v.h.f. (2) Compens. (3) Good construction, with circuit. (4) Possibly a rugged aerial; (5) That the gear be well packed and with spares; (6) That the person supplying arrange insurance on the gear; (7) That the gear be all care but no responsibility for the equipment.

It has also been suggested that a v.h.f. beacon be set up at Macquarie Island. The permission for such an installation would have to be sought through the P.M.G.'s Department and through the Director of the Antarctic Division. If a beacon were to be set up I would like it to be installed under a separate call sign from my own. I feel this could be worth while, if you're interested please do something about it, quickly.

—Rodney Champness, VK6UG.

P.S. When at Macquarie I will be VK6UG.

## DX QRO—NOT ON NET CHANNELS

Editor "A.R." Dear Sir,  
With summer and 33 Mc. DX very close I and many others have some concern regards mobile DX.

Mobile nets have waxed and waned several times over the years, but with increased importance of V.C. nets and the ready availability of complete mobile units suitable for 33 Mc. a.m. conversion, we now have two large and important nets formed on 33.53 Mc. and 33 Mc. These are primarily mobile nets and in S.A. even the majority of base stations are using units identical to those installed in cars and on motor-cycles. A reasonable harmony exists because of accepted net procedures and similarity of power levels for most equipment. However, it is not the local operators which concern us, but those due to DX when it arrives.

When the band opens, local mobile to mobile and/or base contacts will cease due to higher signal strengths from the DX stations. Consequently many of the mobiles will not only prefer, but be forced to use interstate channels, since they are all crystal controlled on one or both of the net frequencies. The co-operation between the mobiles will be of no avail, with all their net procedures, it even one higher powered v.o. control station commands the net frequency. Would any considerable operator, having tuneable equipment at his disposal, deliberately and continuously use a net frequency whilst some mobile stations have to sit and wait because they cannot shift from their frequency like as he has on to theirs? Whilst signals are good, surely they have as much right, and possibly more, to their net frequency than the one who occasionally puts his v.o. on the net allocations.

May I, on behalf of the many net limited mobiles and crystal controlled bases, plead to the v.o.'s with valid Bertha to find some other spot than 33.03 or 33.53 Mc. to use? Surely such a gentleman's agreement is not too much to ask of those few who can help, or hinder, the process and limitations of net operations.

Perhaps it may be helpful to remind net operators of the use of the different channels in different states. Where possible it may be advantageous to include the alternate net, if necessary by diode switching of crystals, even if only for the DX season. A number of VK3 mobiles have been known to have switched to the DX, so perhaps 53.1 Mc. may be a help to VK2, 2 or 7, and an occasional call may produce amazing results if an opening occurs.

Can you, on frequency each Monday to Friday, 1440-1710 C.S.T., just in case something happens.

Hoping co-operation helps, best DX.

H. J. Harvey, VK3ZRE.

## SWITCH

TO SAFETY

# PROJECT AUSTRALIS

Following a request from Project Oscar, the V.F. group for Australia has been assigned to a HI-KCZ. This is in line with the Oscar policy that Amateur Radio satellites should not identify themselves with any national group, but should be representative of Radio Amateurs throughout the world. There will be two to three HI's transmitted by Australia during every ten second identification period.

Some problems have developed in the construction of the flight model of the 144.580 Mc. telemetry transmitter for Australia. While these difficulties are now being overcome, it is expected that the delivery date for the satellite to Project Oscar in California will drop into January next year. All other systems of Australia are working well.

Don Graham VK6SHK has been appointed Oscar State Co-ordinator for Western Australia, succeeding Wally Howie VK2ZAA, who has resigned because of increasing business responsibilities. We wish to thank Wally for his hard work on both the Oscar and Australia Projects, and we hope that he will continue to take an active interest in Amateur Radio satellites.

Project Oscar have advised us of the operating frequencies of the Euro-Oscar 1 metre transmitting satellite. The input frequency will be 144.10 Mc. and the output centre frequency will be 145.800. The translator output will be about 1 watt p.p.s. and the pasband will be wide. It is expected that the Euro-Oscar satellite will be launched into an Oscar III-type orbit, about 500 miles high. The approximate launch time will be 10.00 a.m. as the satellite has still to be tested by Project Oscar, and a 433 Mc. beacon installed.

There have been several enquiries about the names of the VK State Co-ordinators for Oscar and Australia. These are listed below. New South Wales—Alex Swinton, VK3AAK. Victoria—Bill Rice, VK3BPP. Queensland—Laurie Blair, VK4BQ. South Australia—Brian Tideman, VK3TN. Western Australia—Don Graham, VK6SHK. New Zealand—Peter Smith, VK2ZAA.

The Project Australia address is: Astronautical Society, Union House, University of Melbourne, Parkville, M. J. Victoria.

# A & R TOROID BALUNS

General Specifications: Power ratings—Types A, B, C, 300w or 400w p.p.s., provided the a.w.p. is less than 3 i.l. 48 db attenuation—Products are toroids encapsulated with epoxy resin and silica under vacuum. Suitable for use in cold to sub-zero temperatures. Toroids available, and 350C are provided with antenna insulator support brackets. Balun dimensions approx. 3 in. diam. x 1 in. plus socket and lug. Weight approx. 4% to 6 oz.

Type 28A—Impedance ratio 1:1. 75 ohms unbalanced to 75 ohms balanced. 3 to 30 Mc. For use at centre of folded dipole antenna with co-axial cable feed line or at base end with 75 ohm twin lead. Co-axial connector—Type 28A. Price £16/8 and lug terminals. Price £3/7 (inc. S.T.).

Type 33A—Impedance ratio 1:4. 75 ohms unbalanced to 300 ohms balanced. 3 to 30 Mc. For use at centre of a folded dipole antenna with co-axial feed line at base end with 75 ohm twin lead line connector and terminals as 350A. Price £2/7 (inc. S.T.).

Type 35A/35B—Type 35A as 350A except frequency range 500 kc to 5 Mc. or to 30 Mc. for receiving purposes only with increased attenuation. Price £3/7 (inc. S.T.).

Type 36B—This is a type 350 with a co-axial socket 80-350 (Amphenol screw type) connector. Price £4/30 (inc. S.T.).

Type 35A—Type 351 with 40-350 co-axial socket. Price £4/30 (inc. S.T.).

Type 35C—Impedance ratio 1:1. 1. 80 ohms unbalanced to 80 ohms unbalanced. 3 to 30 Mc. For use with 75 ohm mobile whip antenna, coupled to fixed or adjustable transmitter output impedance. Lug terminals. Price £3/40 (inc. S.T.).

Type 35C—Impedance ratio 1:1. 1. 75 ohms unbalanced to 80 ohms unbalanced. 3 to 30 Mc. For use with 75 ohm mobile whip antenna. Price £3/40 (inc. S.T.).

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# SIDEBAND TOPICS

I am frequently asked what future developments can be expected in the field of Amateur S.S.B. Transceivers. The main brands, Swan SW350 and Galaxy V, have been on the market for almost two years. New and radically different models may soon be brought out, what about full transistorisation?

Well, there is no doubt that in the long run, another 3 to 5 years' time, we shall see things change that way. But the changeover is not a simple process. Several hundred watts peak-output is now considered normal and still hard to get with transistors, if at all. It will always require proximity to a solid, heavy-duty power source. The only transistorised S.S.B. Transceiver now available, the SBE34, still uses tubes in driver and final. So will the Japanese product, which is now almost a year behind schedule, and they are still chasing the bugs out of the prototypes!

Replacing parts of the set with transistor circuits makes only sense if one gains something with it, space-saving or reduction in power consumption. A transistor VFC has no merit as such, still requires a large coil box and certainly complicates temperature compensations. So the conclusion is that for a number of years to come the cheaper popular makes will still be with us as they are now, except for possible minor circuit improvements.

When this appears in print I may still have a few new Swans and Galaxies at the old prices in stock, but they are moving fast now and the new supplies that are sailing will have to suffer price increases (see my August issue advertisement).

SWAN/GALAXY 5-banders, with H.D. supply/speaker units	\$600
GALAXY duo-band, 40/80 m. full output, ideal for mobile . . . . .	\$225
HY-GAIN triband beams: TH3JR, \$100; TH6DX, \$200.	
HY-GAIN verticals: 14AVQ, \$50; 18AVQ, \$75, yes, all prices are going up.	
CDB/ALLIANCE rotators, 220/230v., \$200 to £55.	
DC-DC mobile supplies, \$100 and \$120. Automatic keyers \$70.	
WEBSTER Bandspanner mobile whips, complete, 10-80 m., \$50.	

## USED, RE-CONDITIONED EQUIPMENT

WAGNER 1A 10-80 m. S.S.B. Transceiver, with Wagner a.c. supply/speaker unit . . . . .	\$350
GALAXY III 80/40/20 m. S.S.B. Transceiver, VOX unit included	\$325
Perfect EDDYSTONE 888-A 160-10 m Hamband Receiver, A.M./S.S.B./C.W.	\$225
LM-14 Frequency Meter and lots of excellent gear, estate of the late VK2ADC, see Ham-Ads in this issue of "A.R."	

Prices quoted are net, cash with order. If you cannot pay cash, do not consider hire-purchase buying at exorbitant interest and legal charges! See your local branch of the Bank of New South Wales for a personal loan at normal bank interest.

# SIDEBAND ELECTRONICS ENGINEERING

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## \* TRANSCEIVERS, TR1986-7

115-145 Mc. Employs heterodyne exciter in tx. TT15 p.a. Single xtal locks Tx and Rx on same frequency. In-built modulator. Supplied with 4.80 Mc. xtal. \$30, circuit \$1.

## \* MARCONI TF1101 R/C OSCILLATOR

20 c.p.s. to 200 kc., 1% distortion, current model. \$240.

## \* SR550 DUAL CONVERSION COM. RECEIVER

160 metres to 6 metres, Amateur Bands only. 3.5 Mc. xtal band edge marker, xtal supplied, product detector for a.s.b. \$240, 10% discount for cash.

## \* SCR523 V.H.F. TRANSMITTER/RECEIVER

100-150 Mc. Complete with tubes, \$28.

## \* PERSPEX SHEET

1/16 inch thick. Size 4 $\frac{1}{2}$ " x 10". \$1 per sheet.

## \* COMMAND TRANSMITTER

4-8.3 Mc., 5.3-7 Mc. Complete with tubes, \$15.

## \* TR161 TRANSMITTER/RECEIVER

Approximate frequency, 200 Mc. Contains 46 miniature tubes, \$30.

## \* 1J160E HIGH POWER TRIODES

120 Mc. full ratings. Heater 10v. 29a., anode max. volts 3000v., anode max. current 1000 mA., r.f. output 2150 watts. \$8 each.

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Communication Receivers, Test Equipment, etc. Call, write or phone. Equipment inspected and picked up at your convenience any night or week-end.

## \* VALVES

EF50, 20c ea.; 7C7, 10c ea.; CV131, 6CQ6, 50c ea.; 6AC7, 20c ea.; 6AL5, 20c ea.; 6C4, 6AM5, 50c ea.; QQE03/12, \$2 ea.

## \* SIGNAL GENERATORS

TE22 Audio Generator, freq. range: sine 20 c.p.s. to 200 kc., square 20 c.p.s. to 25 kc., in four ranges. Output, 7v. p-peak. Output impedance, 1,000 ohms. Price \$42.

## \* METERS, P25 TYPE

0-500 uA., \$3.25; 0-100 uA., \$6.95; 0-1 mA., \$4.50; 0-10 mA., \$4.50, 0-50 mA., \$4.50. Full range of Meters and Multi-Testers available.

## \* CO-AXIAL CABLE

UR70 72 ohms, 3/16 inch diam., in 27-yard rolls, \$2 plus 75c pack and post. in as-new condition.

## \* RAIB COMMUNICATIONS RECEIVER

150 Kc. to 15 Mc. in six bands. B.f.o., etc. Genuine original condition, with a.c. power supply, \$70.

## \* TRANSISTORS

Brand new. OC72, OC44, 2N132, OC86, OC45, 80c each. AT1138 Power Transistor, 30w., Class B, \$3. Also Diodes: OA71, OA81, OA85, 35c each.

## \* SR700A TRIPLE CONVERSION COM. RECEIVER

30 metres to 10 metres. 1st and 3rd oscillators xtal controlled, 3.4-4.0 Mc. tunable i.f., selectable sidebands, 85:1 geared dial, v.f.o. output for transceive operation, selectivity: 0.5, 1.2, 2.5, 4 kc. Internal 1 Mc. xtal calibrator (xtal supplied). Undoubtedly the finest receiver ever to come out of Japan. \$500, 10% discount for cash.

## \* MILLER 455 Kc. PRE-WIRED I.F. STRIPS

Comprises two i.f. stages, ceramic filter, diode detector, 55 db. gain, NPN silicon transistors, d.c. requirements 6v. d.c. 2 mA., size 1 $\frac{1}{2}$  x  $\frac{1}{2}$  x  $\frac{1}{2}$  inch. \$8.70 inc. tax.

## \* TR16A MULTIMETERS

100,000 ohms per volt. Ranges, d.c. volts: 0.5, 2.5, 10, 50, 250, 500, 1K.; a.c. volts: 2.5, 10, 50, 250, 1K.; d.c. current: 10 uA., 1 mA., 25 mA., 250 mA., 10 amp.; resistance: 20K, 200K ohms, 2 megohms, 20 megohms. To clear, \$25.95.

## \* POTENTIOMETERS

Wire wound, 40c each; carbon, 25c each.

## \* RESISTORS

$\frac{1}{2}$  watt, I.R.C., Welwyn, Eire, Ducon, Philips, \$2 per 100.

## \* 1 H.P. 2-STROKE MOTORS

Ohlsson and Rice. Brand new, just imported from America. Weighs only 5 $\frac{1}{2}$  lbs. 9,300 r.p.m., supplied with 3:1 reduction gearbox, output 2,100 r.p.m. Ideal for driving Alternators for Field Days. Fuel consumption 1 pint per hour. \$30.

## ANY QUERIES

Beginners are welcome, ask Jim and Laurie Gardiner any questions. They are Amateur Radio operators and will be only too pleased to assist.

## \* CRYSTALS

Personal shoppers only, \$1 each.

## \* SPECIALS

3AP1 c.x.o. tubes. New in cartons, \$1.25.  
3000 type Relays, 50c each.  
Inter-Office Phones, 15-station type, \$4 each.  
7-pin skirted Valve Sockets, P.T.F.E. insulation, silver plated, only 20c each, c/w shield.  
Speaker Transformers: 7000 ohms to 2 ohms; 10,000 ohms to 3.5 ohms; 50c each.  
9-pin skirted P.T.F.E. Valve Sockets with shield, 50c each.  
Irish Recording Tape, Mylar Base: 150 ft. x 3 in., 75c; 900 ft. x 3 in., \$2.75; 1150 ft. x 8 $\frac{1}{2}$  in., \$3.50; 1800 ft. x 7 in., \$4.75.  
3 uF. 1000v. d.c. Block Capacitors. Only 25c each or \$2 per dozen.

## \* MINIATURE CAPACITORS

New shipment. 600 v.w. Values: 0.001, 0.02, 0.005, 0.0005, 0.0002, 0.0001 uF. \$2 for 80, plus freight.

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April last, the writer of which gives many reasons why he thinks there should not be a change. In fact, as he is personally concerned, after hearing some broadcast operators manfully trying out the new term, we have come to the conclusion that on the whole, it sounds like a subtle digestive upheaval brought about by an unfortunate culinary experiment!

Those who are in a position to attend our monthly general meetings are reminded that the next one will be held at Wireless Institute, Victoria, on Friday, November 23. A lecture on "Solid State Sideband" will be given by Mr. Ted Banstead, an A.W.A. engineer. 73, Ivan VK2AIM.

#### HUNTER BRANCH

A most successful Convention was held during the October long week-end. The activities commenced on Friday night and continued until Sunday, 2nd October. At the monthly meeting members were invited to display and describe some item of home-built equipment and thus compete for a valuable prize; the Radiotron Designer's Handbook. The effort considered most praiseworthy by the judges and the votes of the audience was the 3 and 6 metre transmitter and modulator described by Bill VK2ZWH. However, because of the high cost of the equipment, the Radiotron magazine subscriptions to "Radiotronics" were awarded to the others taking part in the contest. Tony and Ray VK2JF and Gordon Z2SO. The only disturbing point is that only four members could present equipment for judging when perhaps all of us have built some equipment worthy of display at the last convention.

At the Annual Dinner there were fewer guests than usual, but the convivial atmosphere at the hall was a fitting reward for those who assisted and supported the branch. Among the guests were Cyril SCH, who represented the N.S.W. Division, and Ray VK2HC. The welcome to the visitors was given by Bill XXT and Ray IHC proposed the toast to the Institute. The address was given by Cyril SCH who commended the Branch on the standing it holds with the Divisional Council.

An interesting address, outlining the progress of Amateur Radio in the Newcast area was given by Lionel SCH, who spoke at length about activities of both past and present members. There was a social and a musical success and the choice of venue proved to be a wise one. In addition to a tactically prepared programme and menu, a large number of informative literature was presented to each of the diners.

On Sunday, 2nd and 3rd October, the Field Day was held at the Bolton Point. Attendance early was disappointing but by early lunchtime a representative crowd had gathered and

entrants for the events numbered more than six in each case. Once again, Dave 3AWZ proved to be an outstanding competitor with a win in the second two metre hunt and an unbelievable score of 21 contacts in the half hour afternoon scramble. The 80 metre transmitter was unfound although it produced a very loud signal throughout the hunt. Winner of the afternoon 1 metre hunt was Greg Partridge, the Bud 00, of YVU. In addition to the mobile events there were two pedestrian transmitter hunts on 2 metres. These resulted in wins for David Fraser and Michael Korach. David is a member of the Westlakes Radio Club while Michael is a Gosford member. Since the regulations regarding rifles have been relaxed, a rifle was conducted with a "Radiotron Designer's Handbook" as a prize. Much to his own and the audience's delight, the book was won by Otis Z3I and this and other prizes were presented at a short ceremony on the ground. At this time it was announced that all proceeds would go to the I.T.U. Fund as a Hunter Branch contribution. So seriously does the branch consider the situation of international pressure on our exclusive allocations that a census of members was taken and all asked agreed on the direction of all funds towards the cost of representation at that allocation. It is believed that a sum of about \$40 will be added as a result of the field day profits. Another field day has been planned for Sunday, 4th December, and once again all profits will go to the I.T.U. fund.

Harry 1AFA has increased his activity since being visited by Paul Linke, a very kind short wave listener. Apparently Paul paid Harry several visits and by some means or other was able to convince him to get back on the air. The added activity of the bands caused by irregular operation becoming regular can only help the cause of the hobby. There are some who would have us out of the r.f. spectrum altogether if a case could be brought for our exclusion. So help preserve the hobby by operating as frequently as possible on as many bands as you are able. Jan Z2JO has become the proud owner of a high power rig originally owned by Jack Z2Q. Jack now operates sideband exclusively and passed on the excellent rack-mounted gear to Jan. Watch out for some high power shortly, thanks to Jack. Paddy Z2AU was heard on the air recently after a long absence caused by a failure of some power

supply. And Jim Z2HT is widening his field by adding some local contacts. It is good to hear Jim on the air with the local boys and he certainly has a fine signal on s.s.b. Sherwood Z2AF, Len Z2FD and Cyril SCH recently hit the headlines with a picture in the "Herald" and as a result Sherwood has made a vow to be on the air by the time this appears in print. We see Susan Z2B and Charles Z2L are the latest to acquire carphones for 148 MHz, and there soon should be additional QRM on this frequency. And, perhaps best of all, "Bones" Medford is applying for his licence while Bruce Morley is preparing for the big quit. Good luck men, the sooner you are on the air, the better. And, as they say on the films, that just about wraps it up for now. Don't forget the November meeting on Friday, 4th, at the usual venue. Ian Ferguson, of "Electronics," will be there and rumour has it that he will be talking s.s.b. Don't miss it! See you 73, JAEK.

#### CENTRAL COAST BRANCH

The last meeting of the Central Coast Branch was held on September 18. Lionel Doonan VK2EDL, well known as an instructor at Gore Bay Technical College, gave a most interesting lecture on Printed Circuits which seemed to emphasise how apt the term "wireless" was. It was about the difference between the American and Australian pronunciation of the word "solder." The American version comes out as "sodder."

The annual Field Day will be held at Gosford around the middle of February with all the usual attractions plus something new. Keep an eye open for the exact date which will be published in a few weeks.

The Branch Christmas Party will be held on December 7 at the new Blair Restaurant in William Street, Newcastle. A delicious smorgas-bord "punish" is planned, to be preceded by "punch" conversation, etc. 73, Mona VK3AXS.

#### SUMMERLAND AMATEUR RADIO CLUB

The bi-monthly meeting of the club was held at Lennox Head on 20th September. Members present were Gordon 1A0E, Graham 8GU, Ted Z2K, Hilda Z2Q, John Z2Q, John Z2KA, Fred Z2F, Jack Z2BG, Lindsay Z2CO, Kevin Z2SW, Ken Z2KH. The main item of business

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#### LECTURE TAPES

16. "Telly Ho." 7 Mcs. Fox Hunting, 1 hr. with slides, H. Burtoft, VK2AAH.

17. Cause and Chance Creation, 40 min. No slides, Prof. Monism.

18. Grid Dip Oscillators, 80 min. 15 slides, Bob Winch, VK2OA.

19. Balun Transformers, 2 hrs. 33 slides, Joe Reed, VK2JR.

20. "How does my Signal go?" 70 min. 19 slides, Frank Hine, VK2QL.

Details in August "A.R."

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was a notice of motion given by our president, ZACQ, to change the name of the club from the Far Northern District Radio Club to the "Summerland Amateur Radio Club." This was dealt with and the result was that we are now known as the "Summerland Amateur Radio Club."

Some apologies were received from members, namely Blue 2AKU, Harold 2AWH and Bob 2AAS.

A good day was had by all present and the next meeting, the annual meeting, it was decided to hold at the QTH of Lindsay ZACQ, our President, on the 25th November. Members please note this date and all roll up.

Band activity has not been very good, especially on the 3.6 Mc. net every Thursday night at 8 o'clock, so what about it, chaps, blow the dust out of the rig, put some sizzle on the air.

Once again I am plugging for the Kings-cliff get-together on 29th November, so please make a special effort and attend, you will be assured of a good time.

The notes this month consist of mostly pleas and dates, promise I will do better next month. 29, George ZACQ.

— . . . —

## VICTORIA

### I.T.U. ACKNOWLEDGMENTS

Further donations received are as follows—  
\$5.00: F. Dettman, 3AFJ.  
\$5.00: L. L. McInnes, 3AMK; R. K. Smyth, 3AKL; A. K. Fielden, 3AKD; S. McIndoe, 3ATD.  
\$4.00: G. E. Vincent, 3AGV; G. Luckman, 3ADL; A. Moran, 3ABQ.  
\$3.00: J. A. Ferguson, 3AXL; D. Volpert, 3ABC; E. Blake, 3ZHA; L. Poynter, 3ZGH; G. Chalmers, 3ARG; R. Torrington, 3TJ; M. C. Foster, 3COI.  
\$1.00: M. Lodge, 3JM; I. Smith, Assoc.; M. Dalton, 3DY; K. Duff, 3CV; E. C. Phillips, 3AEP; A. Lord, 3ZE.

## EASTERN ZONE

Shortly 3BC will be moving to Stratford, and from all reports he is a keen V.H.F. fan and will be heard most likely on Channel A 2 Lm. Barry 3ZQC at Mirboo North, has moved in from Western Victoria and works at Ch. 2, is another 3 Lm. fan, and is attempting to get his Pye going on 3.032 Mc., the TX is okay but the Rx won't receive. Joe 3YO is another recent arrival on 3 Lm., after many years off the bands, and Dave 3ZCZ has also come up on 3 Lm. as well as 3 Lm. Les 3ZSS, of Moa, is a new member of the Amateur fraternity and is active on 3 a.m. What about giving him a call you 2 metre fellows.

Albert Cash and George 3ZCG are working on some super-regen. equipment for 423 Mcs. Albert hopes to go for his ticket in October, so all the best Albert. Sorry to report that there is no h.f. news, as I haven't had the time to listen to the 20000 hr. hook-up on 80 of a Friday, because I'm down in the city all week and only have the week-end free.

I have been transferred from 3GI to the Antarctic Division and am doing familiarisation courses before sailing to Macquarie Island in early December. I hope to take gear for most bands, 80, 40, 30 and 6 metres in particular, and s.s.b. if that is possible. Don't forget if you hear Macquarie don't forget to give a yell. Is there a volunteer to carry on this task of keeping the Eastern Zone on the map as far as notes go? I will endeavour to glean notes until the end of the year if anyone can send me some in rough form. George 3ZCG has supplied me with a good proportion of the v.h.f. news for which I am most grateful. 3UG.

— . . . —

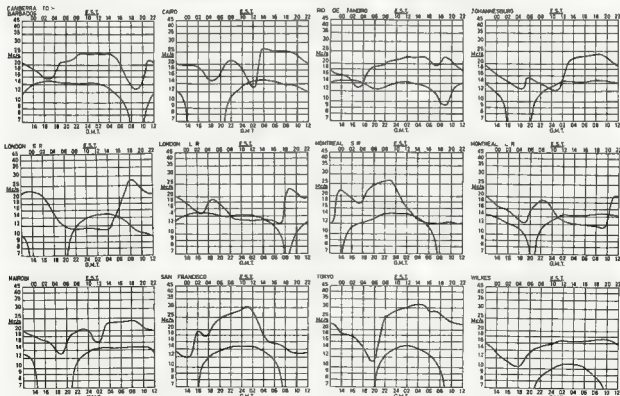
## SOUTH AUSTRALIA

The monthly general meeting of the VKS Division for September was held in the club-rooms to an attendance of members and visi-

tors well over the 70 in number, despite the inclement weather. Very little business, either Divisional or Federal, was discussed, although the Federal Councillor, Geoff. RTV read out a letter sent to the VKS Division protesting on their action over the new Federal constitution, and judging by the comments which followed the reading, the members present thoroughly approved of its contents. Details were also given of the coming large-scale W.I.C.E.N. exercise which will be held over the long week-end of October, and will be the latest in date, with 24 stations participating in a v.h.f. net covering the area from Port Pirie to Murray Bridge. George 3RX then took over with the distribution of QSL cards, and after a short smoke-on the meeting was handed over to Messrs. Judd and Farrell, from Teknionix Australia Pty. Ltd., whose subject was naturally oscilloscopes, and what oscilloscopes they were, making the old faithful 58P1 seem like the lace-up boot era. The first unit demonstrated was flat from d.s. to 50 megas, and locked on to complex waveforms like the caretaker's Alsatian elephant would like to lock on to the seat of my pants at the end of the meeting. Its unique features were demonstrated to an entranced audience, the double time base which allowed any selected portion of the trace to be brightened up for closer examination, fairly laying the audience in the aisles. Having showed the first unit's capabilities, Mr. Farrell then switched on the second unit which displayed some 5 cycles of a sine wave on the screen, usually mentioning that the frequency of the signal was 100 megas. This unit was capable of handling inputs of up to 870 megas, with a sensitivity of 4mV/cm, and with his audience still gasping for breath he then showed how a desired waveform could be stored on the screen for up to one hour on a half screen, whilst another pattern was being stored or displayed on the other half.

Having by now almost stunned the audience with his dexterity at the controls, the lecture was concluded by a film on the production of cathode ray tubes. The voice of

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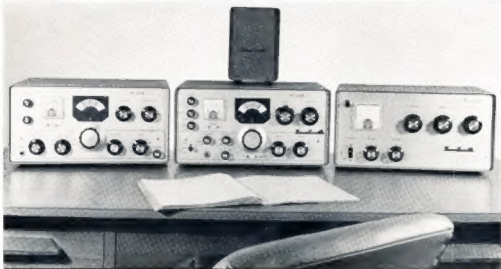
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5 15	30c	50 20	25c
5 350	45c	100 6	25c
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10 6	30c	100 50	75c
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10 35	35c	100 300	\$1.50
10 300	65c	150 120	75c
18 300	50c	200 350 Can	\$1.80
18 525	75c	125 3	25c
20 300	65c	150 6	25c
24 350	65c	200 25	65c
24 500	97c	200 50	90c
25 3	32c	250 3	50c
25 6	32c	250 6	55c
25 12	35c	250 18	55c
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